Column Base Connections: Research, Design, and a Look to the Future

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Professor, University of California, Davis

2022 T.R. HIGGINS LECTURESHIP AWARD

Acknowledgments

Sponsors

- AISC
- Charles Pankow Foundation
- Pacific Earthquake Engineering Research Center
- National Science Foundation
- California Department of Conservation

Acknowledgments

Students

- Ahmad Hassan, UC Davis
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- Ryan Cooke, Schuff Steel
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Collaborators

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- Tomasz Falborski, Gdansk University, Poland
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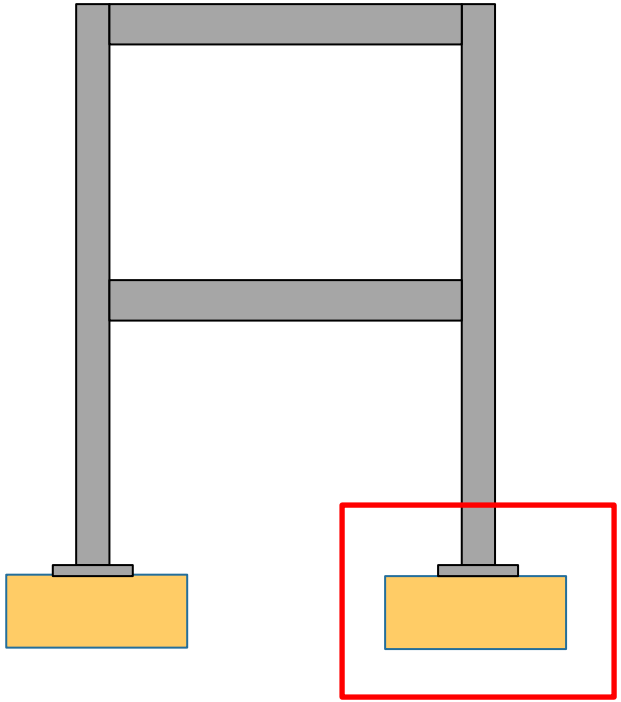
Joel Chandler – Owen Steel Company

Tom Sabol – Englekirk Structural Engineers

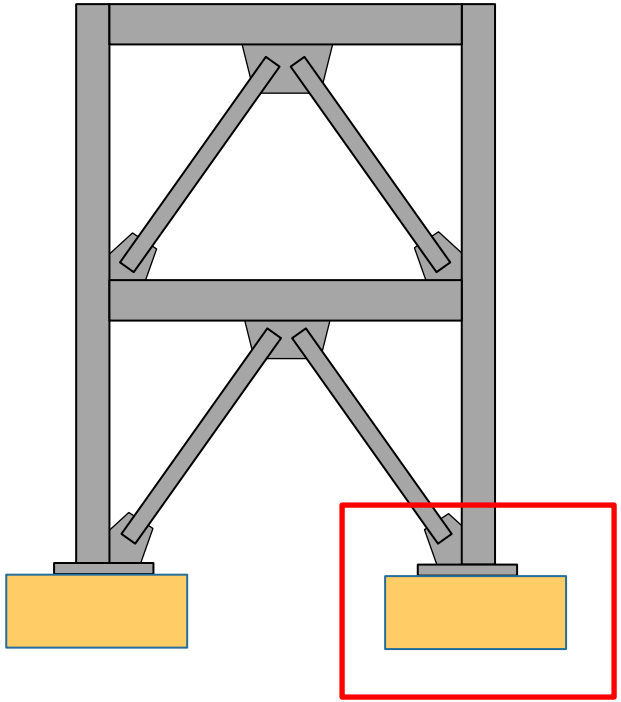
Matthew Eatherton – Virginia Tech

Matt Smith – L&M Industrial Fabrication

Used in all buildings



Used in all buildings



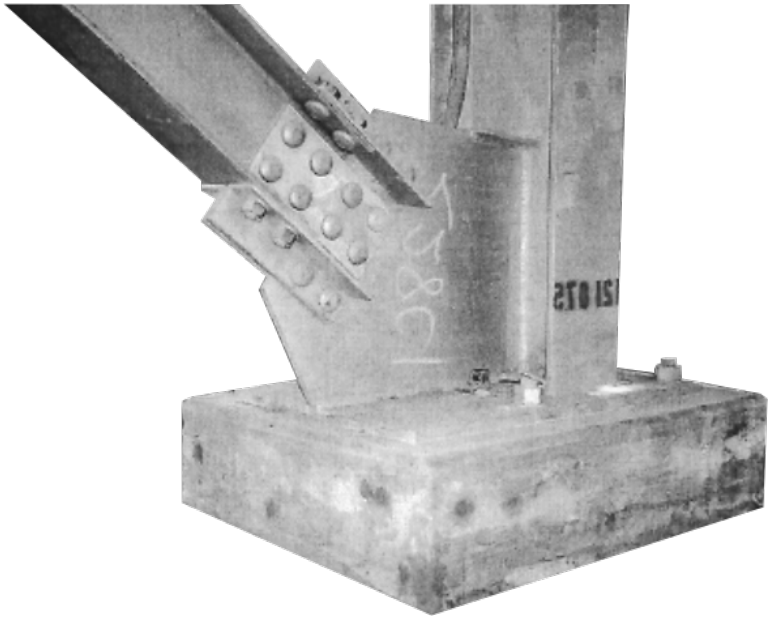
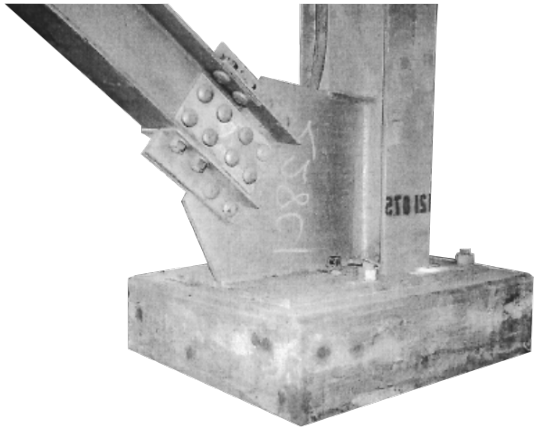
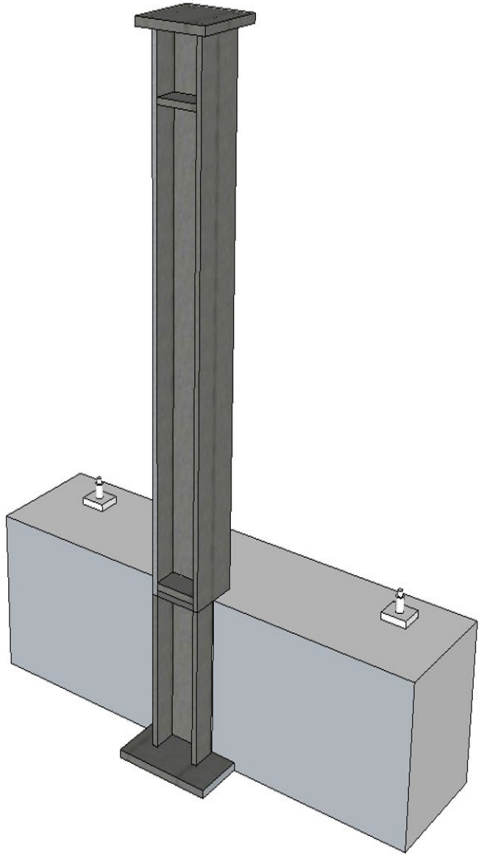


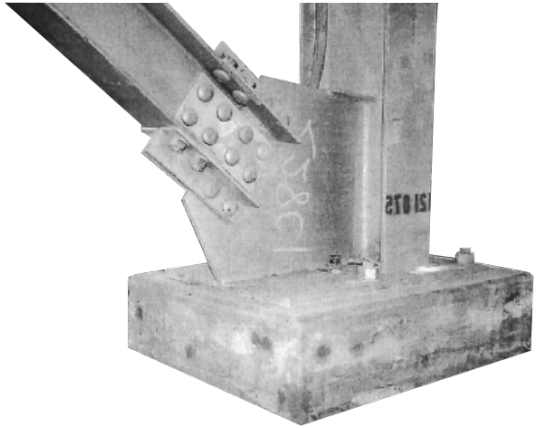
Photo credit: Rick Drake (2003)

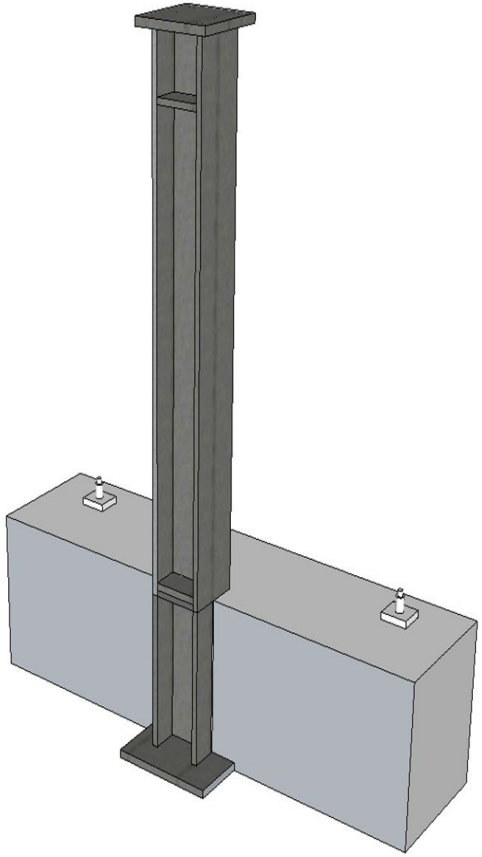
Diversity in details



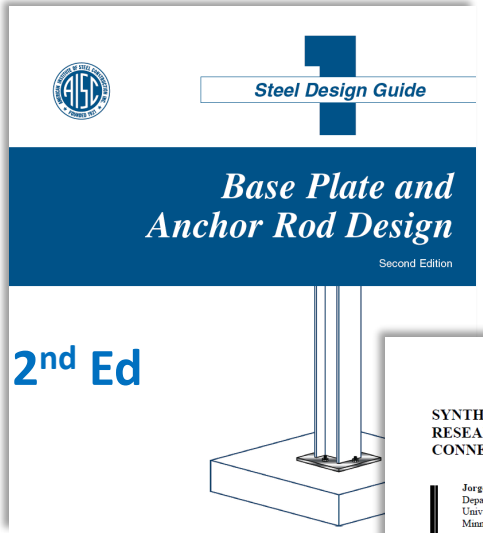


Always at steel/concrete interface

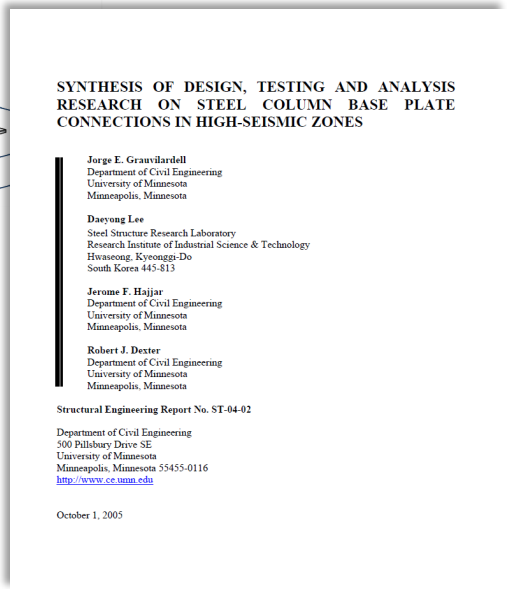




Timeline and scope



2nd Ed



SYNTHESIS OF DESIGN, TESTING AND ANALYSIS RESEARCH ON STEEL COLUMN BASE PLATE CONNECTIONS IN HIGH-SEISMIC ZONES

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Structural Engineering Report No. ST-04-02

Department of Civil Engineering
500 Pillsbury Drive SE
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Minneapolis, Minnesota 55455-0116
http://www.ce.umn.edu

October 1, 2005

2005-2006

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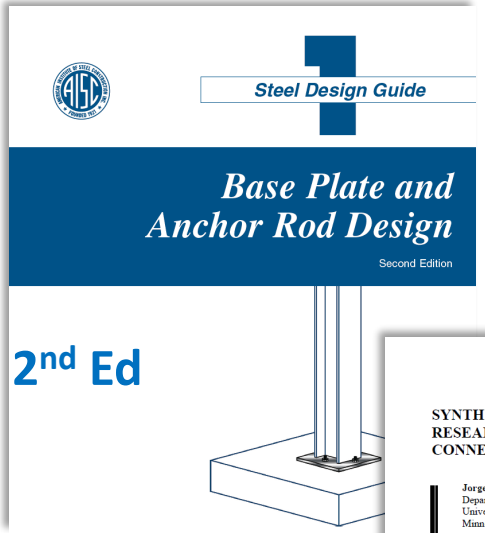

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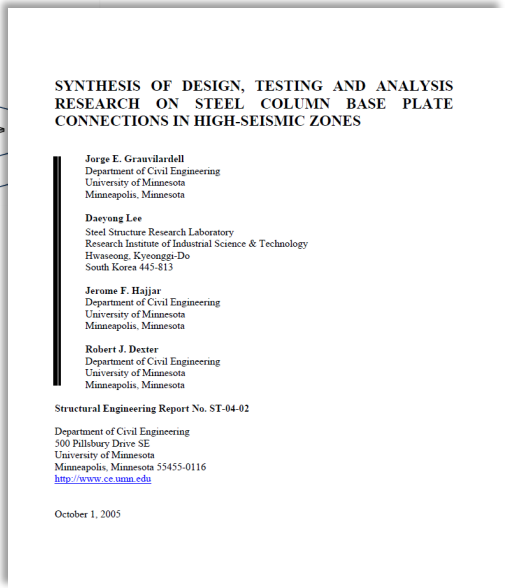

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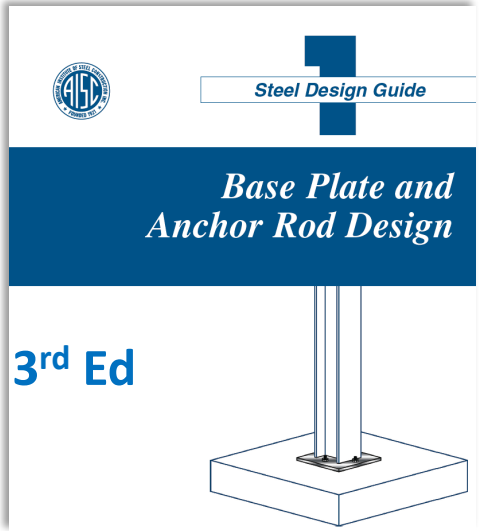
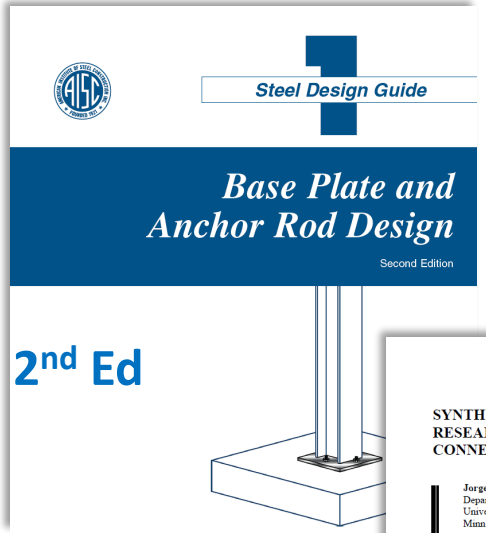


3rd Ed

2024-ish

Timeline and scope



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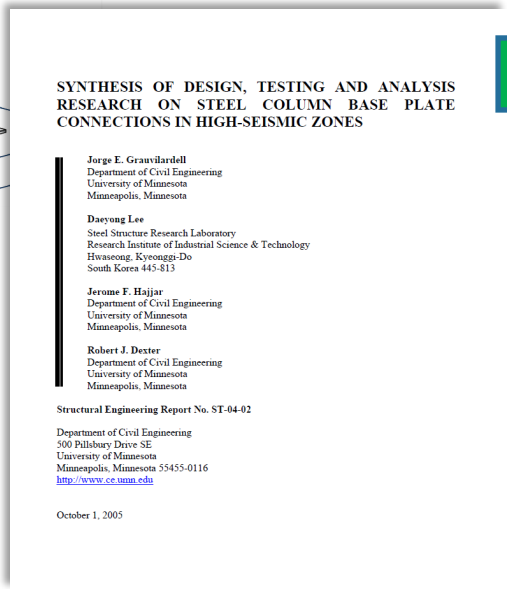
2005-2006



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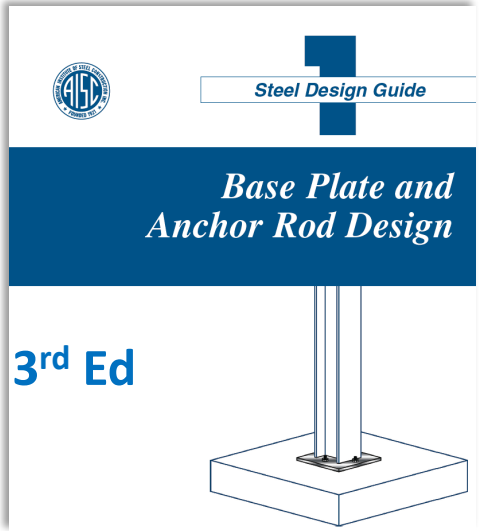
New developments



3rd Ed

2024-ish

Organization

Part 1

Exposed Base Plates

- Prevailing understanding and design methods
- New Developments

~35 mins

Part 2

Embedded Bases

- Prevailing understanding and design methods
- New Developments

~15 mins

Part 3

A look to the future

- "Resolved" issues
- Ongoing work
  Unresolved issues

~10 mins

Organization

Part 1

Exposed Base Plates

- Prevailing understanding and design methods
- New Developments

~15 mins

Part 2

Embedded Bases

- Prevailing understanding and design methods
- New Developments

~15 mins

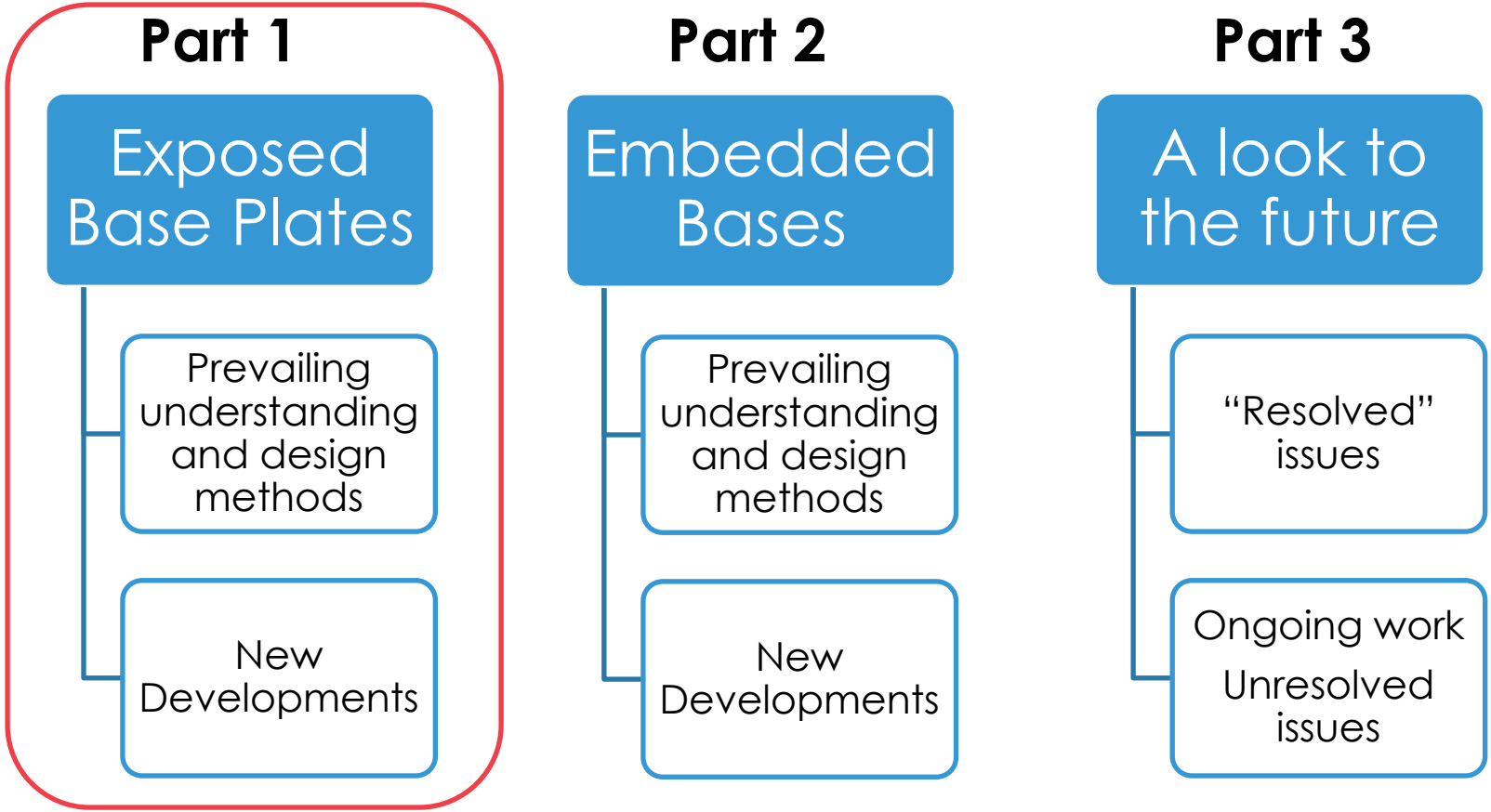
Part 3

A look to the future

- "Resolved" issues
- Ongoing work
  Unresolved issues

~7-8 mins

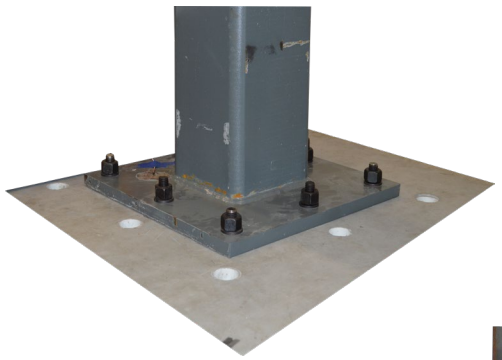
Organization

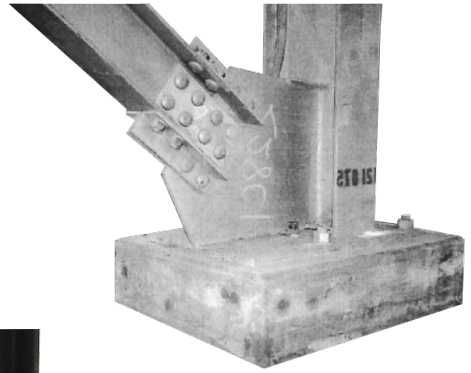


Part 1 – Exposed Base Plate Connections

Exposed Base Plates

- Prevailing understanding and design methods
- New Developments





Part 1 – Exposed Base Plate Connections

Exposed Base Plates

- Prevailing understanding and design methods
- New Developments

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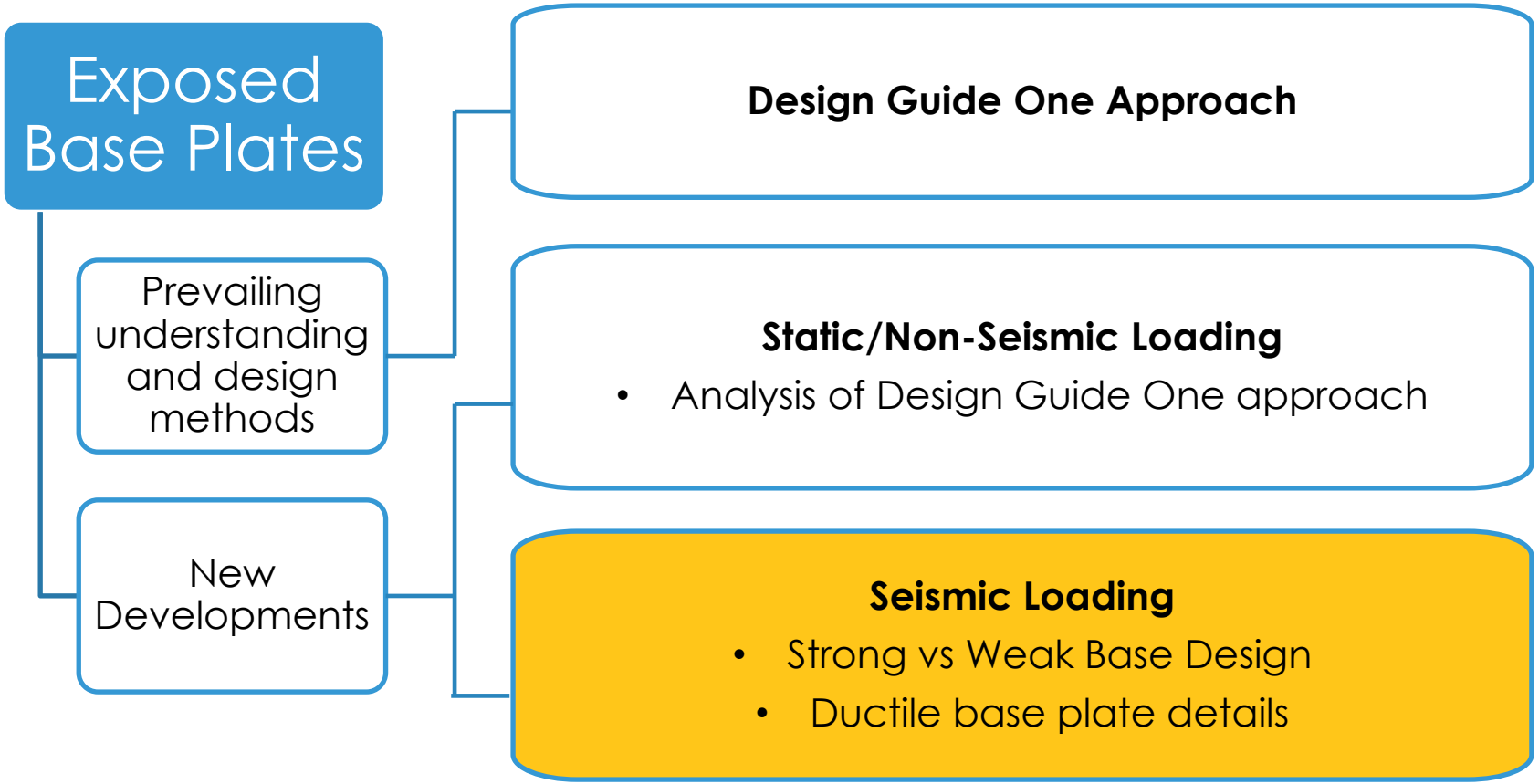
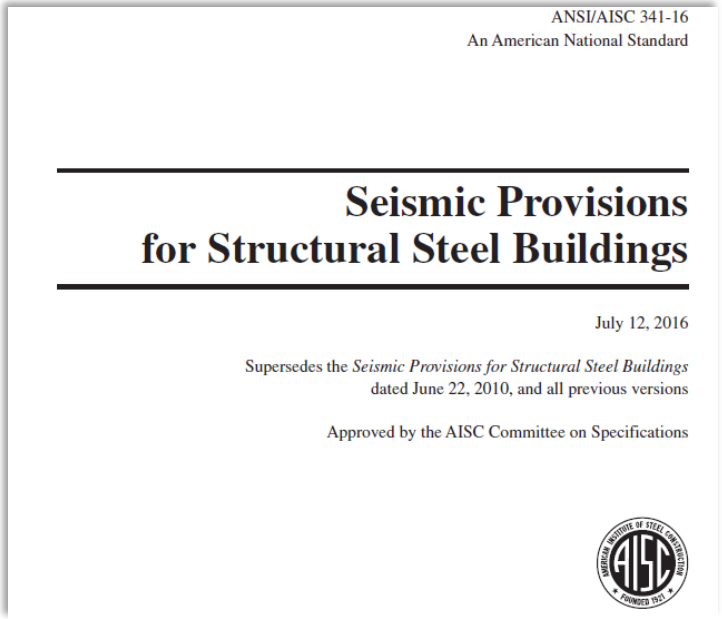


Seismic considerations – exposed base plates

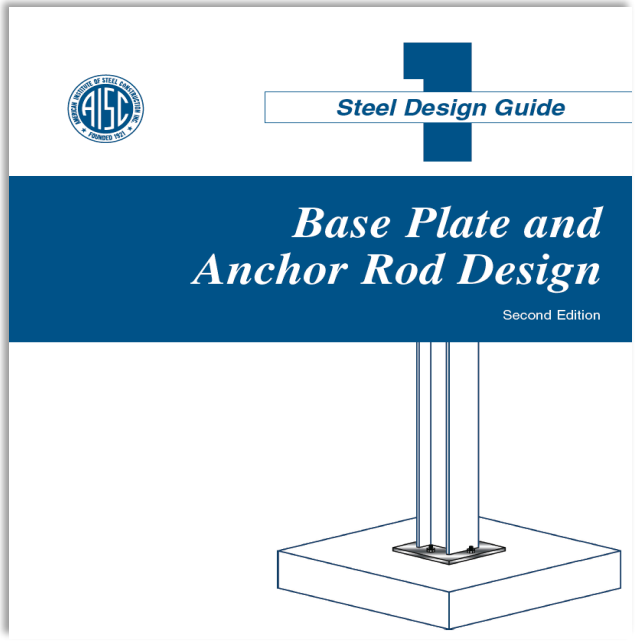

ANSI/AISC 341-16
An American National Standard

Seismic Provisions
for Structural Steel Buildings

July 12, 2016

Supersedes the *Seismic Provisions for Structural Steel Buildings*
dated June 22, 2010, and all previous versions

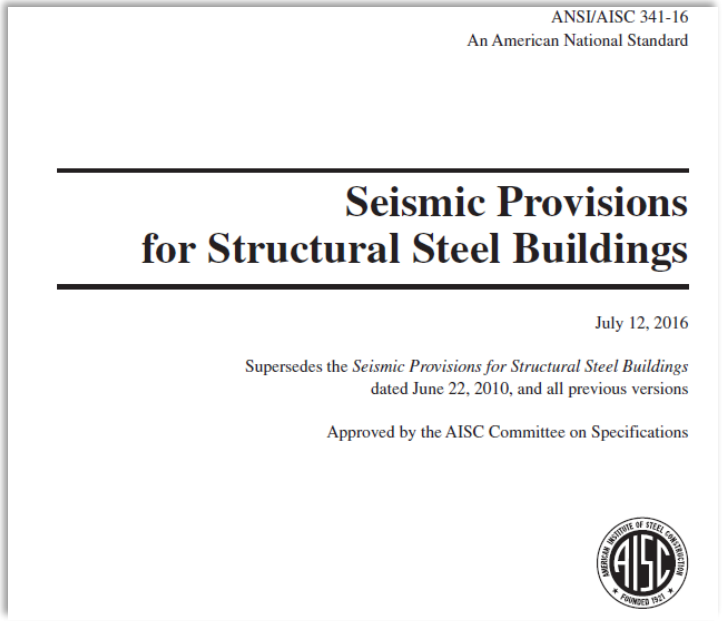
Approved by the AISC Committee on Specifications


Steel Design Guide

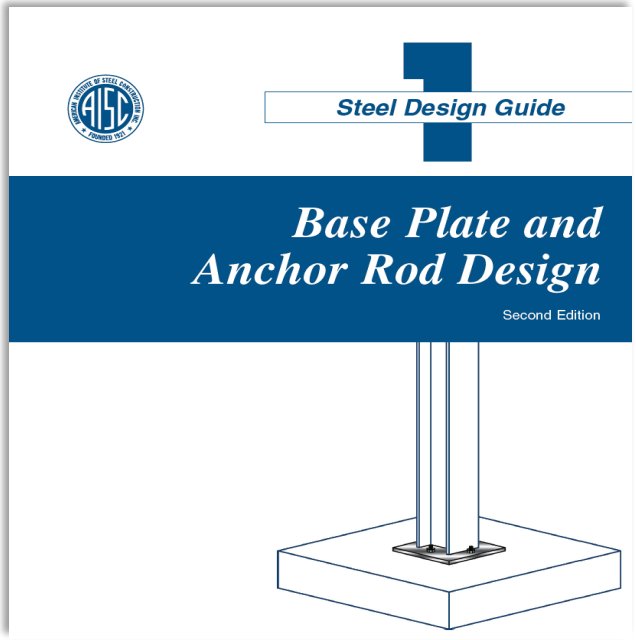
Base Plate and
Anchor Rod Design

Second Edition

Seismic considerations – exposed base plates



Broad principles and philosophy



Design and detailing

Seismic considerations – exposed base plates

ANSI/AISC 341-16
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Seism
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Supersedes the *Seismic Prov*
dated June

Approved by the

6c. Required Flexural Strength

Where column bases are designed as moment connections to the foundation, the required flexural strength of column bases that are designated as part of the SFRS, including their attachment to the foundation, shall be the summation of the required connection strengths of the steel elements that are connected to the column base as follows:

(a) For diagonal braces, the required flexural strength shall be at least equal to the required flexural strength of diagonal brace connections.

(b) For columns, the required flexural strength shall be at least equal to the lesser of the following:

(1) $1.1R_yF_yZ/\alpha_s$ of the column; or

(2) The moment calculated using the overstrength seismic load, provided that a ductile limit state in either the column base or the foundation controls the design.

Broad principles and philosophy

Two ways to design seismic base connections

Strong base design

6c. Required Flexural Strength

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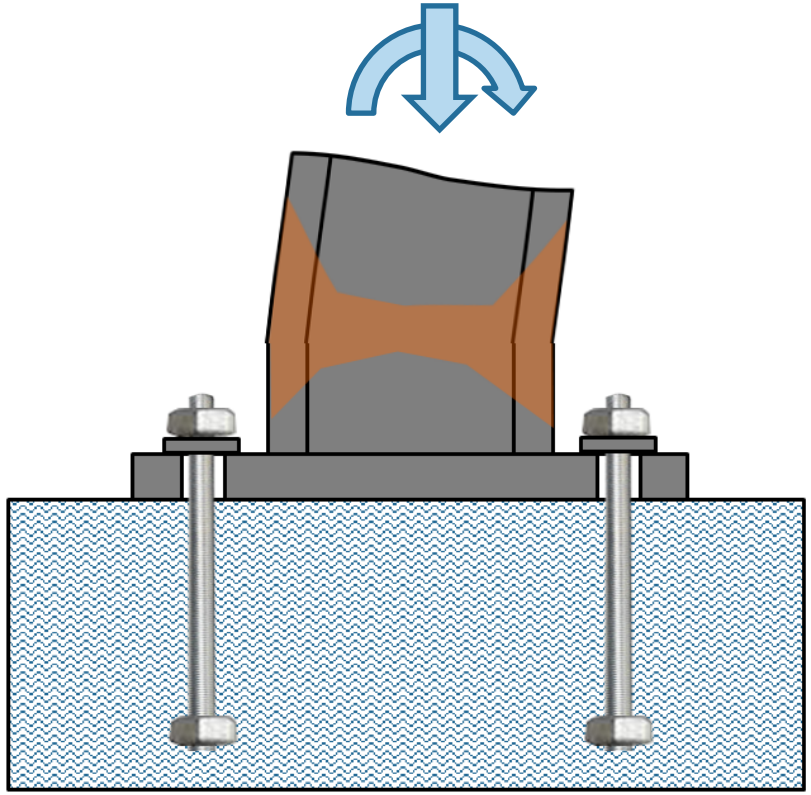
Strong base design

- Direct application of Design Guide One
- Large rods, thick plate



Two ways to design seismic base connections

Weak base design using Ω_0 loads

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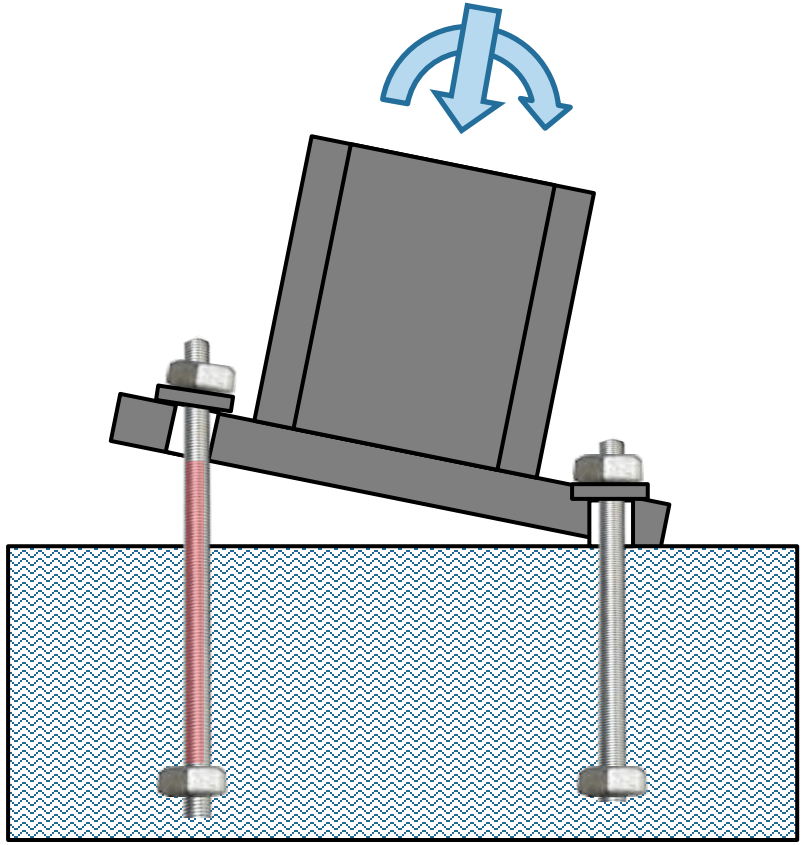
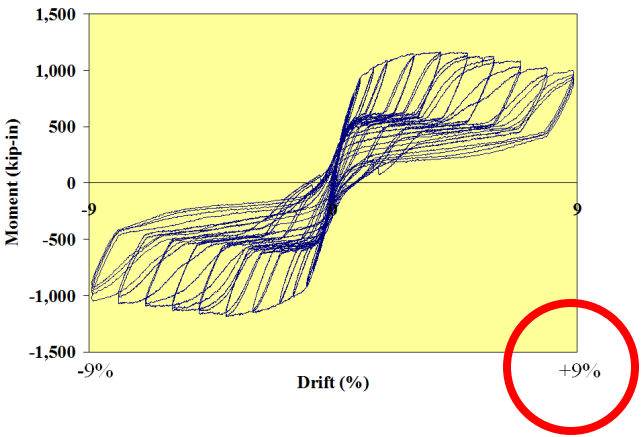
Weak base design

- Weak base design
- Cheaper connection
- Requires ductility
  - Limited specific guidance on how to achieve this



Inherent ductility of exposed base connections

Great inherent ductility (rotation >5%)



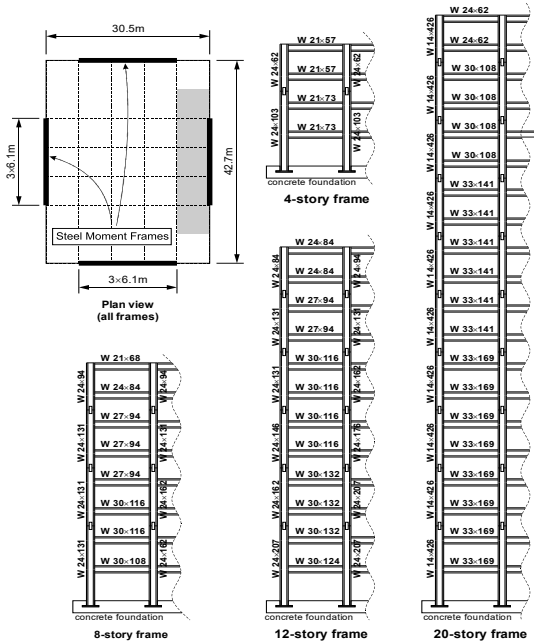
Gomez et al. (2010), Kanvinde et al. (2015), Trautner et al. (2017), Astaneh et al. (1992), Fahmy et al. (1999), Burda & Itani (1999), Lee et al. (2008) and Wald et al. (2020)

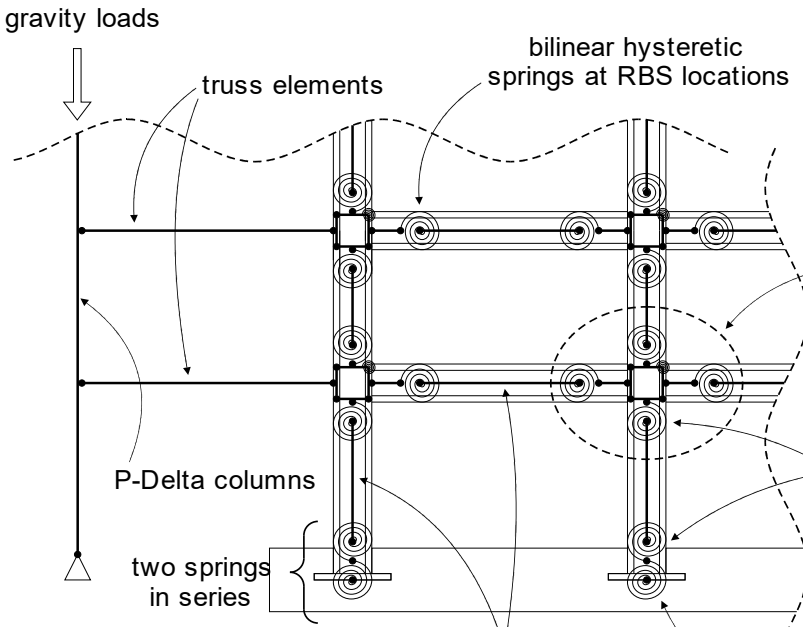
How to achieve weak base design?

- Develop understanding of base rotation demands
- Engineer details that can meet these demands, with confidence
- Demonstrate effectiveness of these details

How to achieve weak base design?

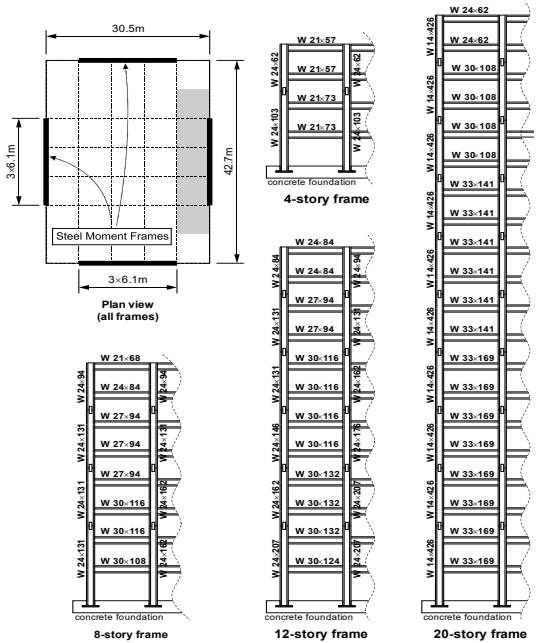
Develop understanding of base rotation demands through NLTHA

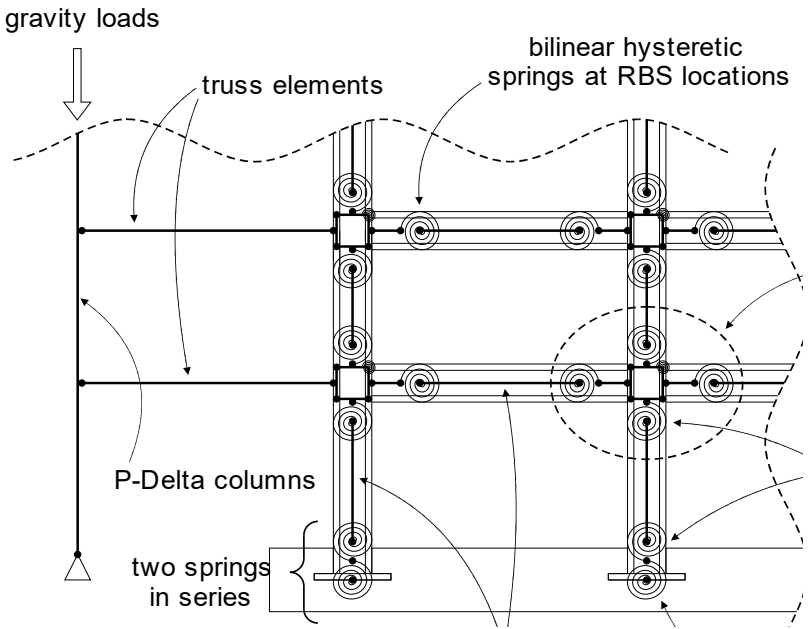




How to achieve weak base design?

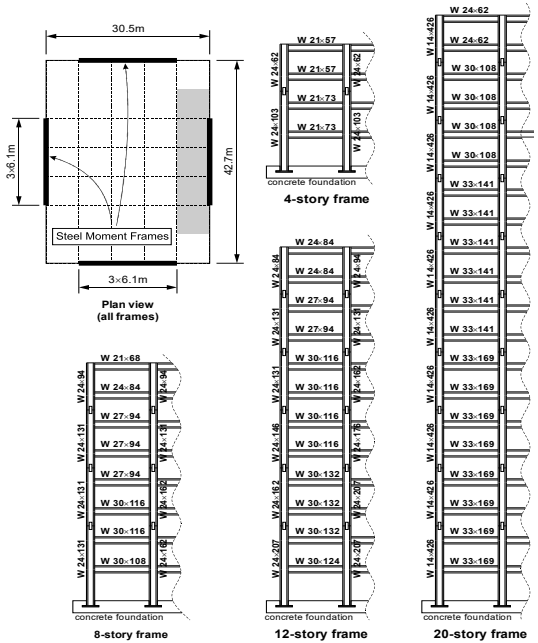
Rotation in the range of 4-5% when designed for Ω_0 loads provides great performance

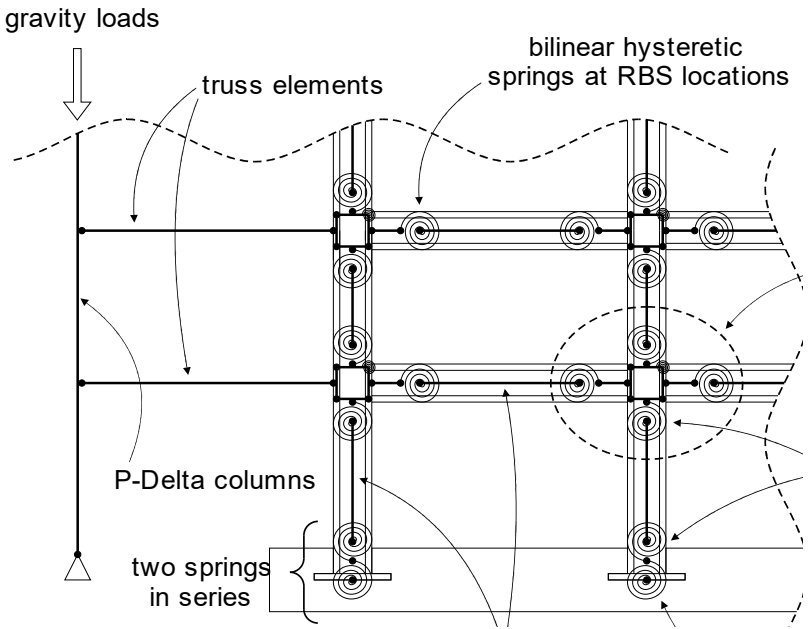




How to achieve weak base design?

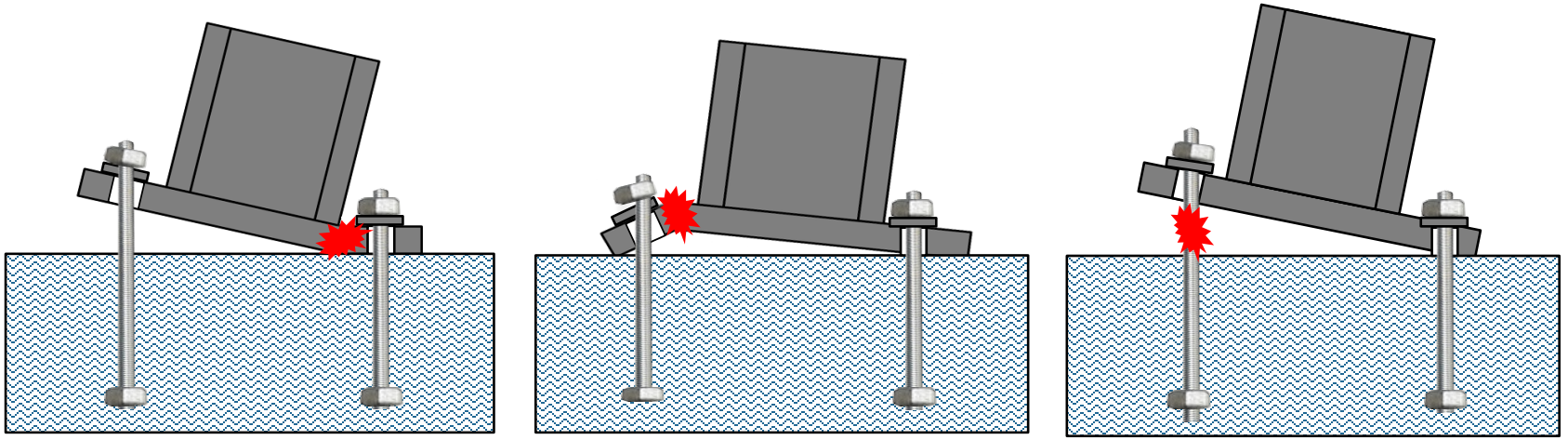
Weak-base design is well within reach



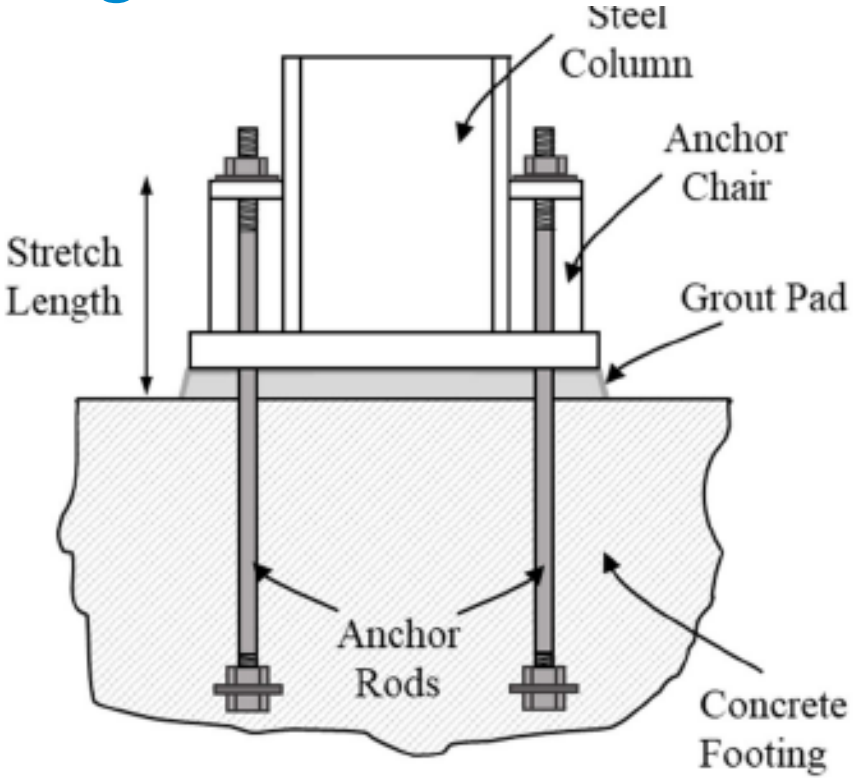


Engineering such a connection

Which ductile mode to use?



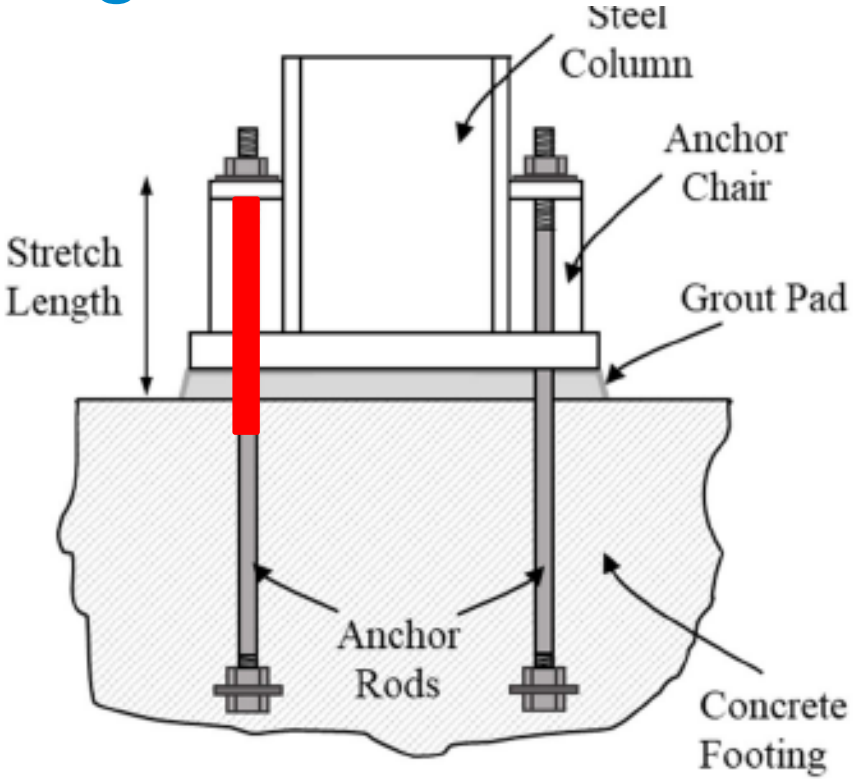
Ductile base connections through rod elongation



Soules et al (2016)

- Good performance observed under high shaking
- Attributed to stretch length

Ductile base connections through rod elongation



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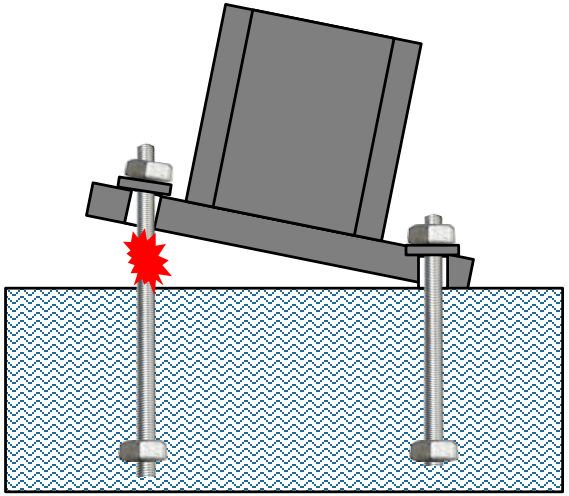
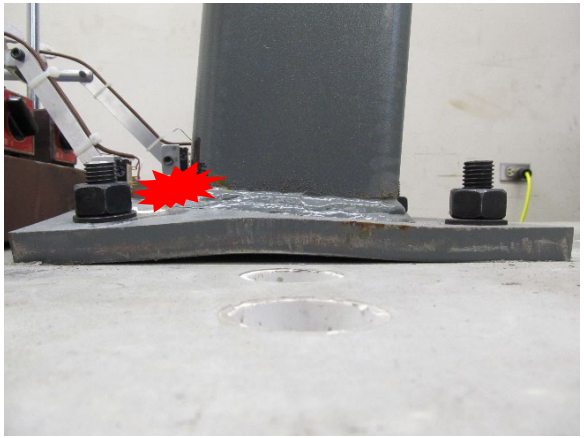
Achieving ductility in base connections

Consensus around rod elongation vs base plate yielding





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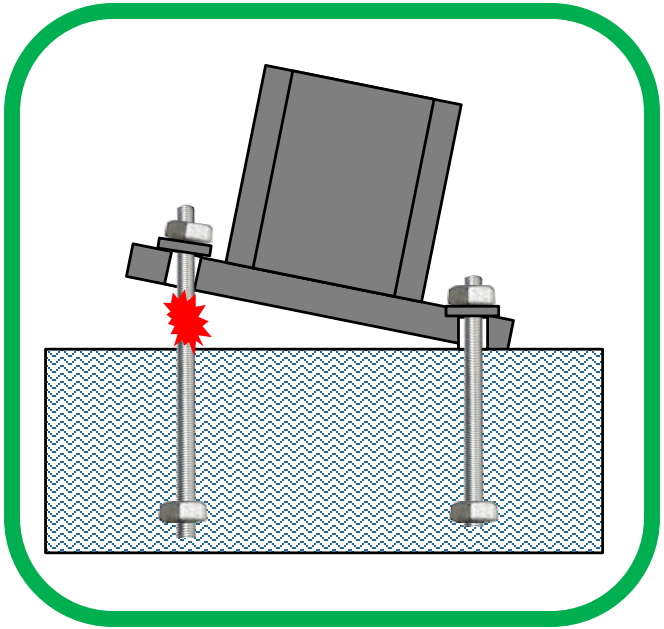
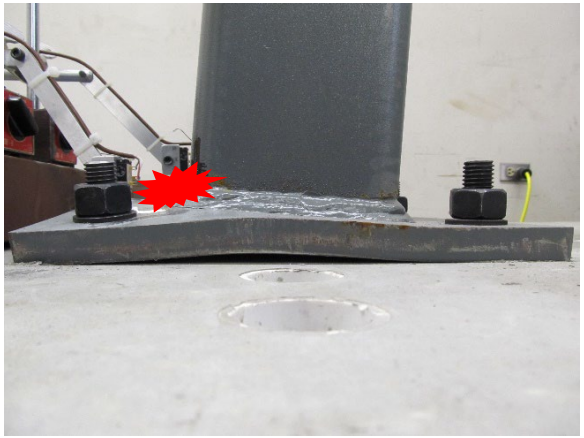
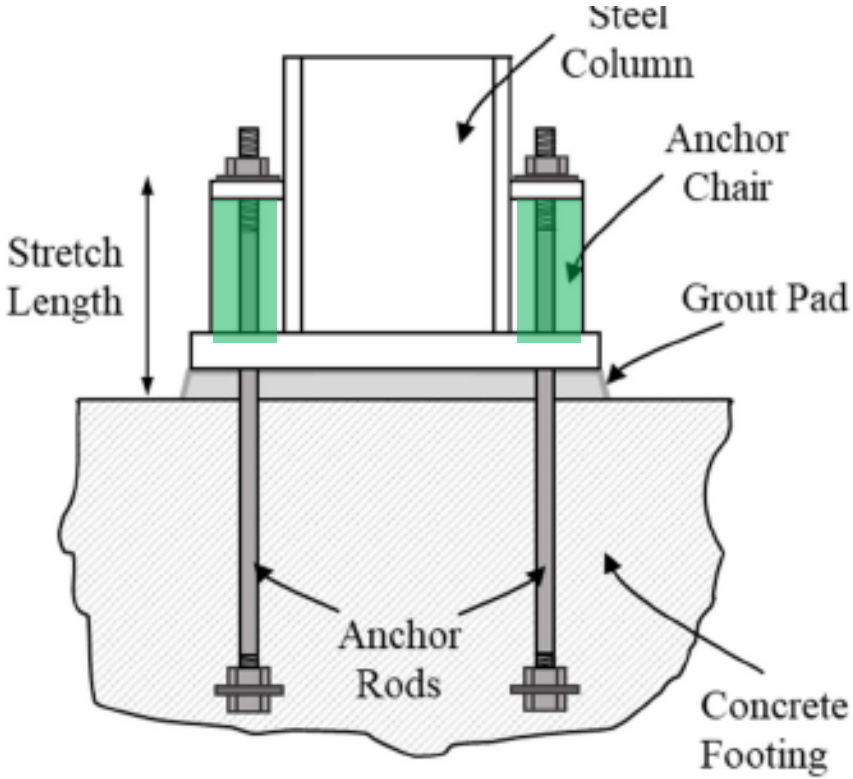
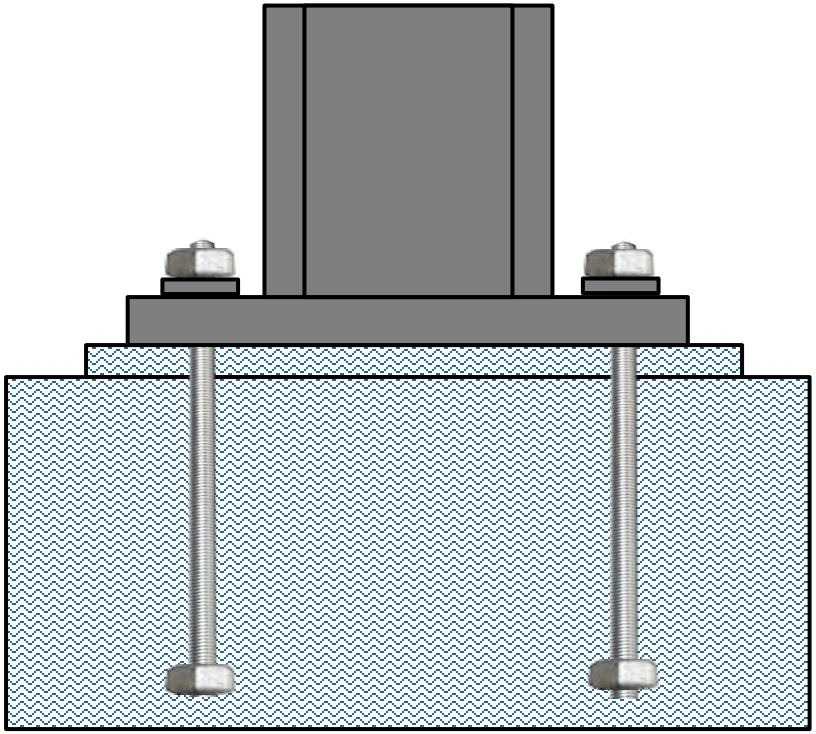




Stretch length requires additional fabrication

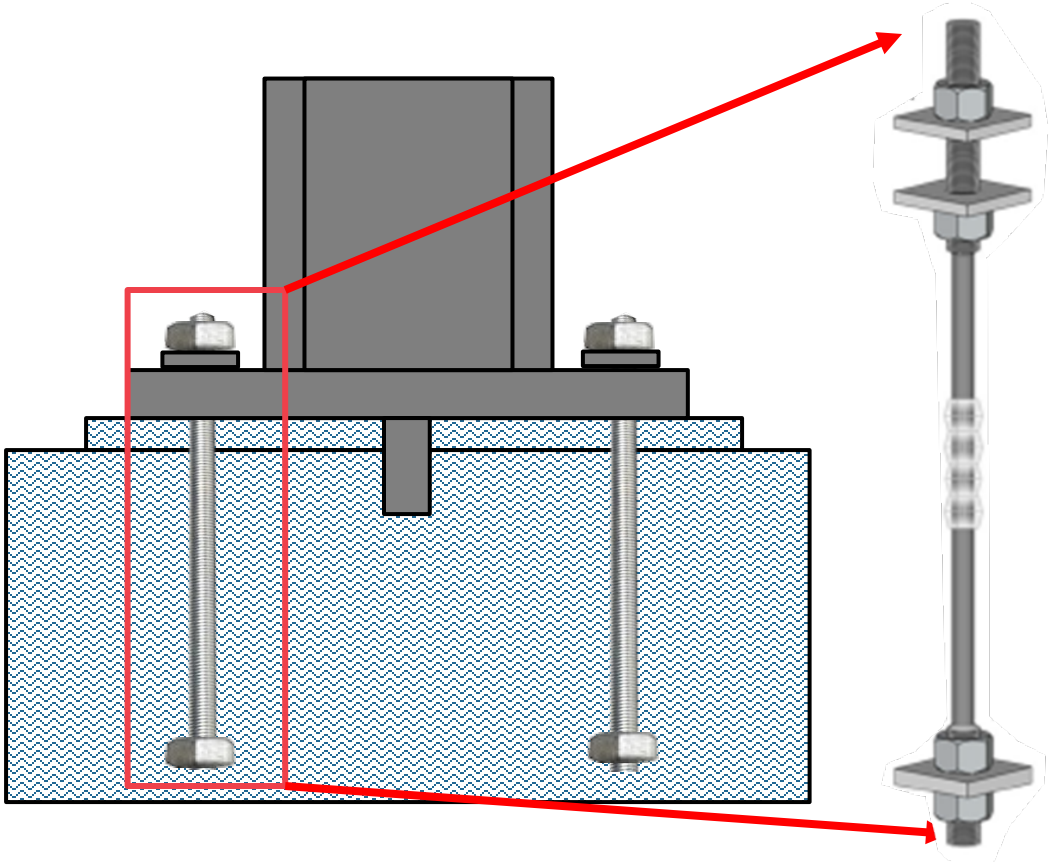


A new “reliably ductile” detail – AISC/Pankow Project

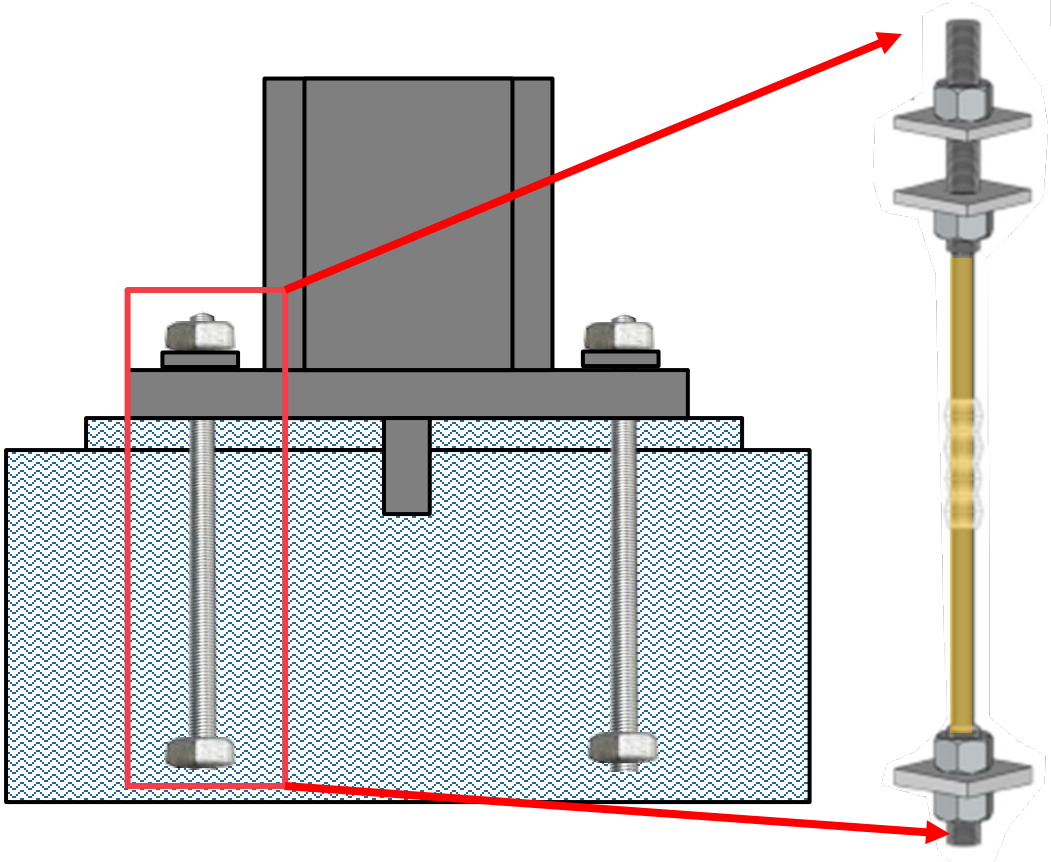


- Consultation with design engineers, fabricators
- Focus on convenience of fabrication
- Minimal changes to existing practice
- High confidence in ductile response

The Upset Thread Detail



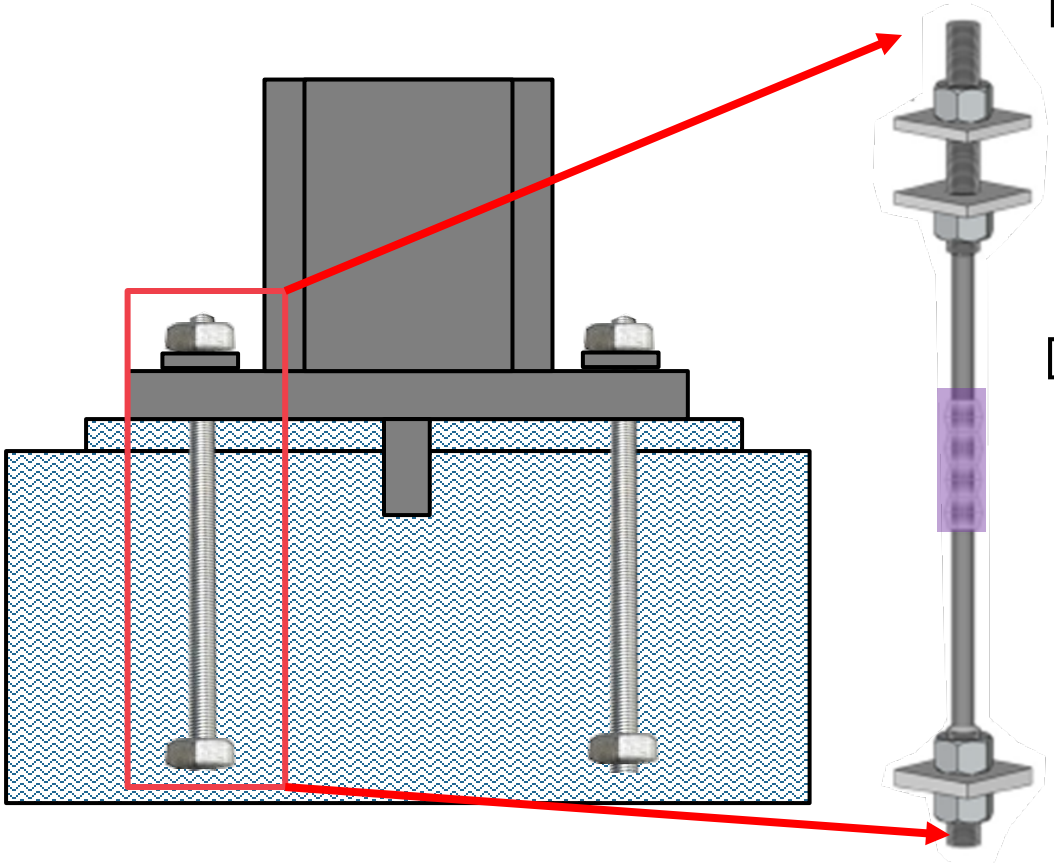
The Upset Thread Detail



Milled down “upset” threads

- Enhance ductility
- Define yielding zone

The Upset Thread Detail



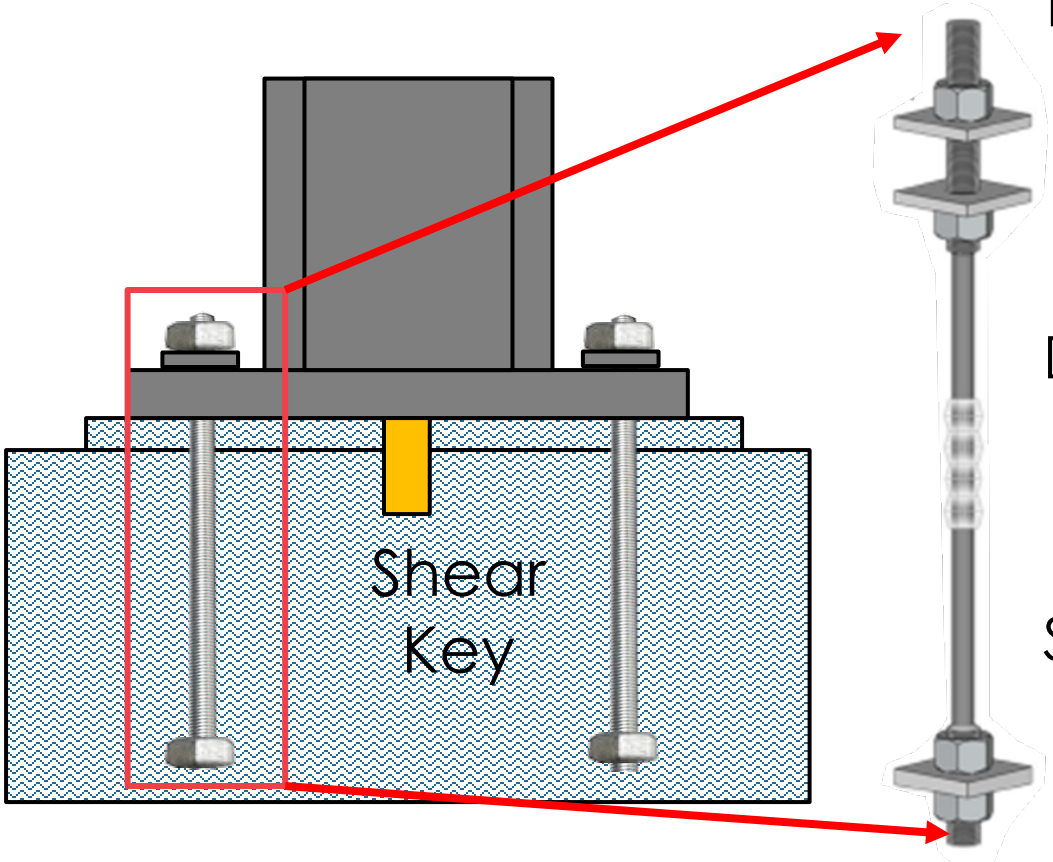
Milled down “upset” threads

- Enhance ductility
- Define yielding zone

Debonding tape

- Prevents rod catching
- Similar to BRB

The Upset Thread Detail



Milled down “upset” threads

- Enhance ductility
- Define yielding zone

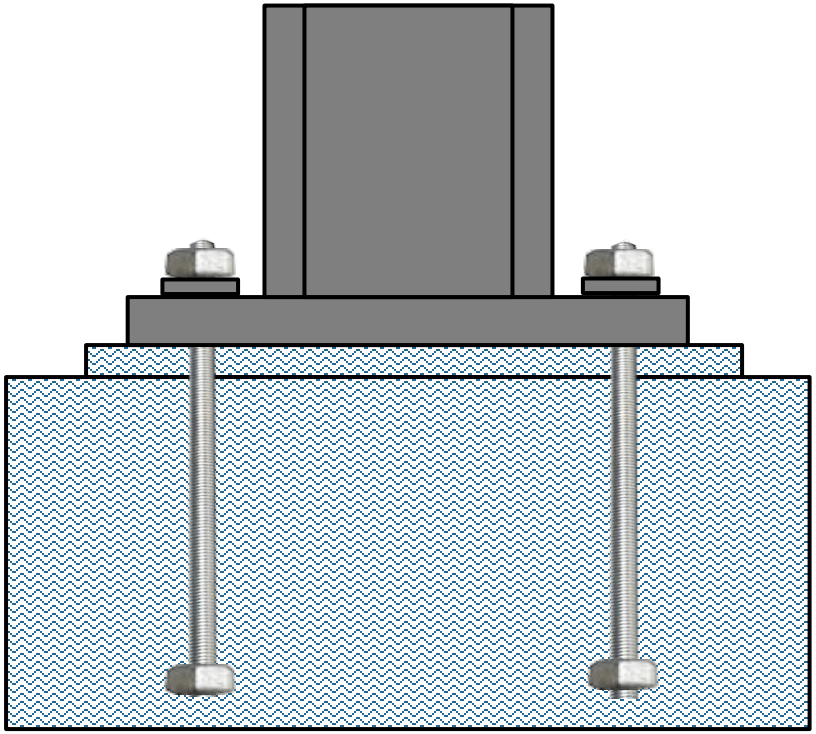
Debonding tape

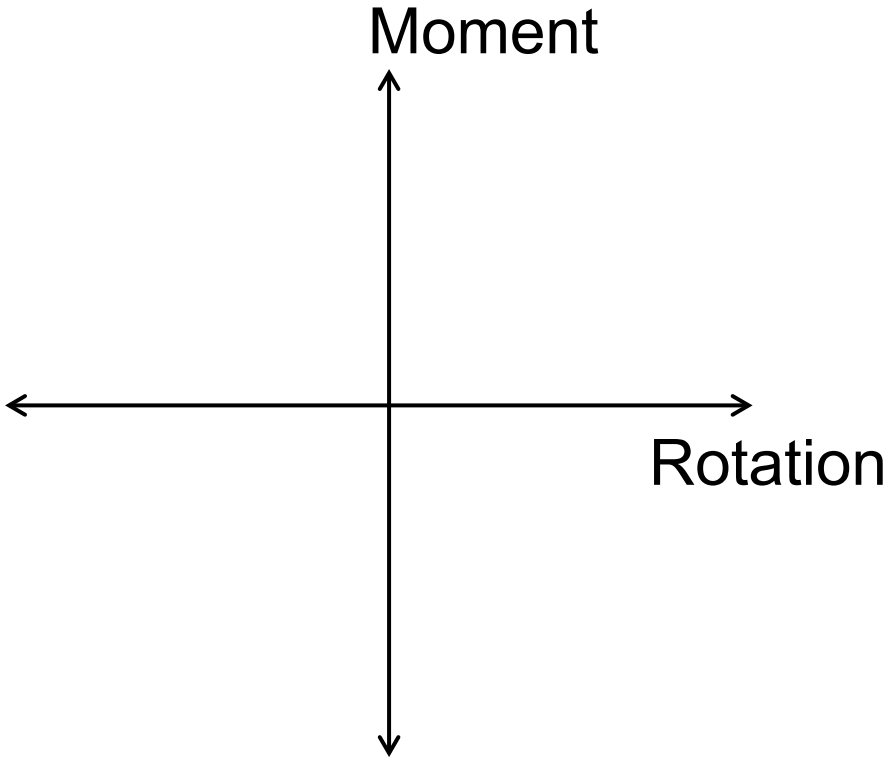
- Prevents rod catching
- Similar to BRB

Shear Key

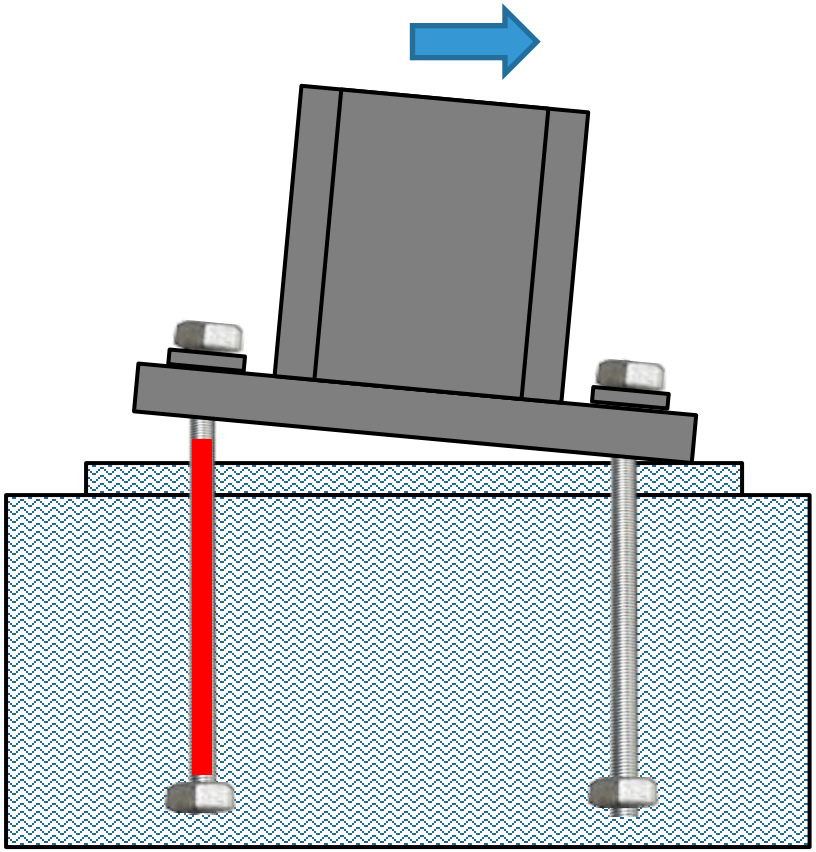
- Protects rods from shear

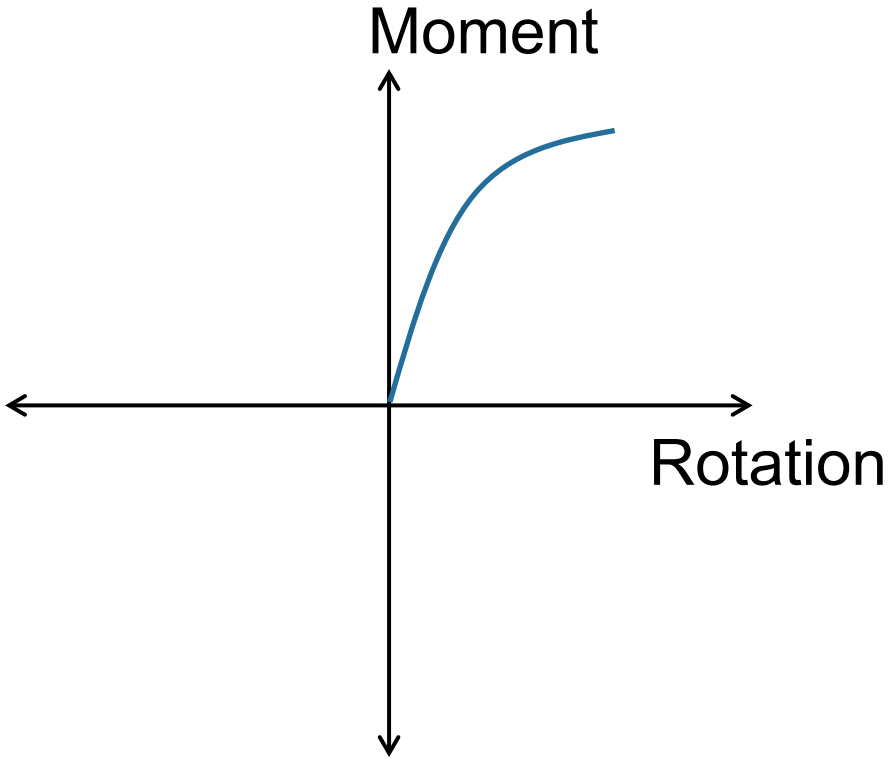
Intended behavior



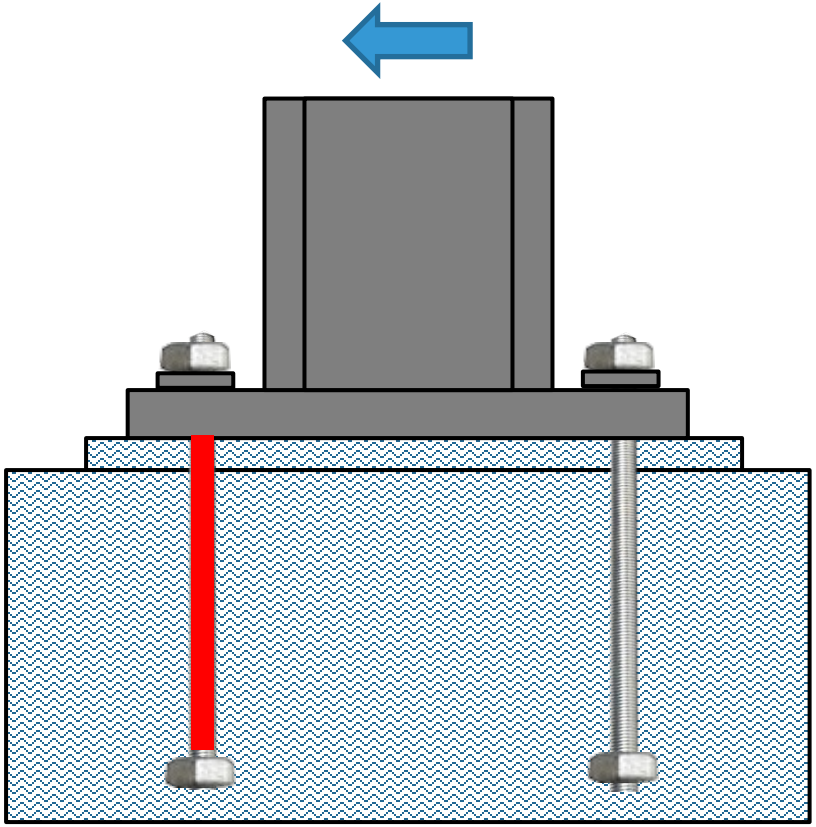


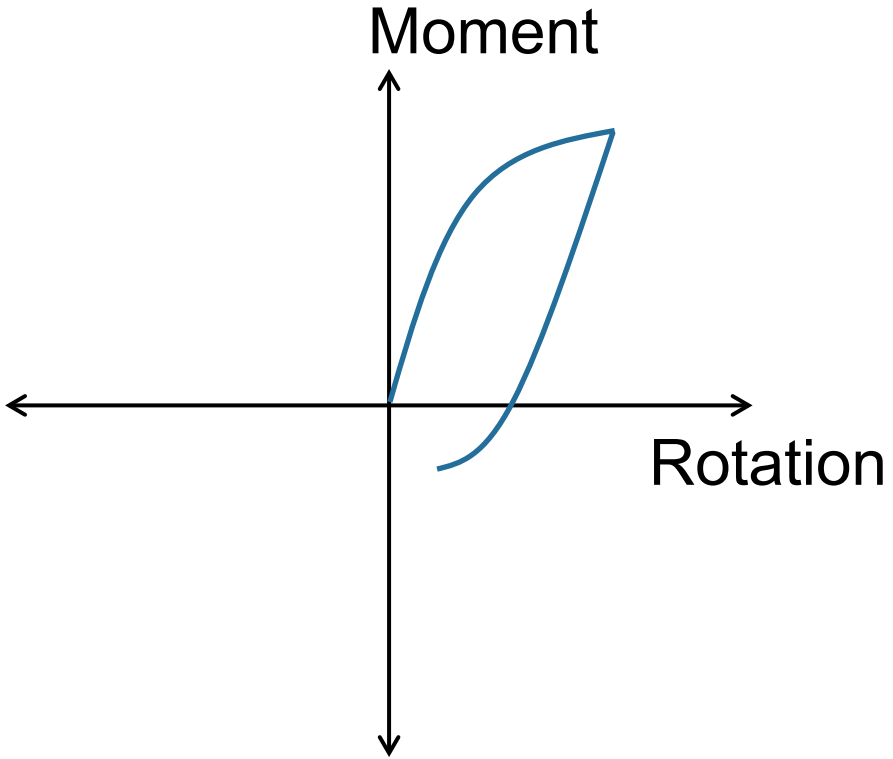
Intended behavior



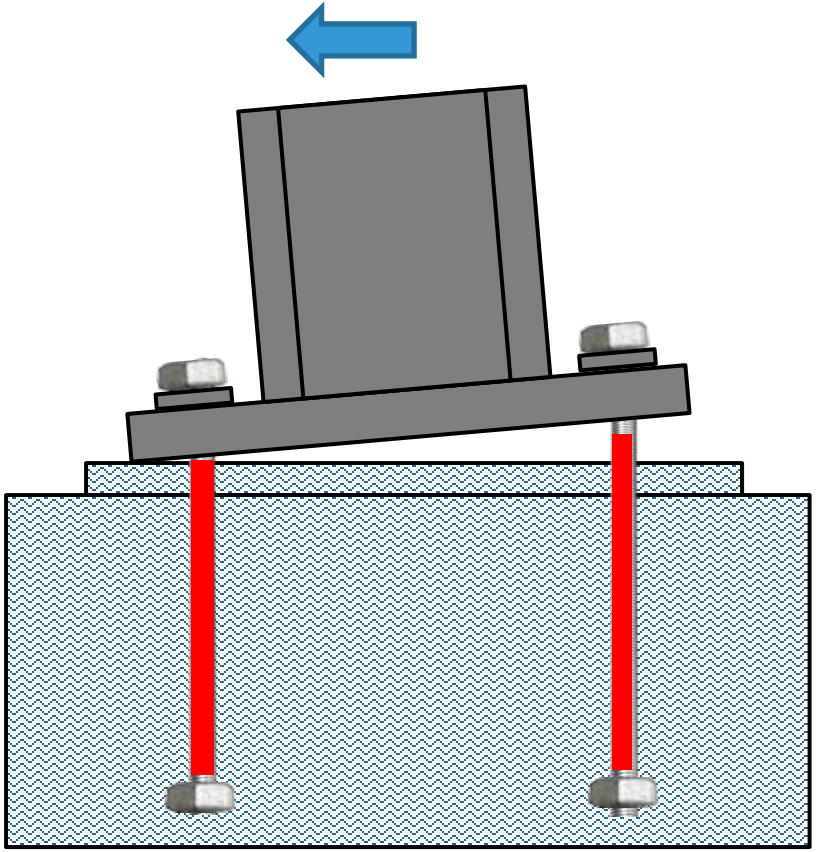


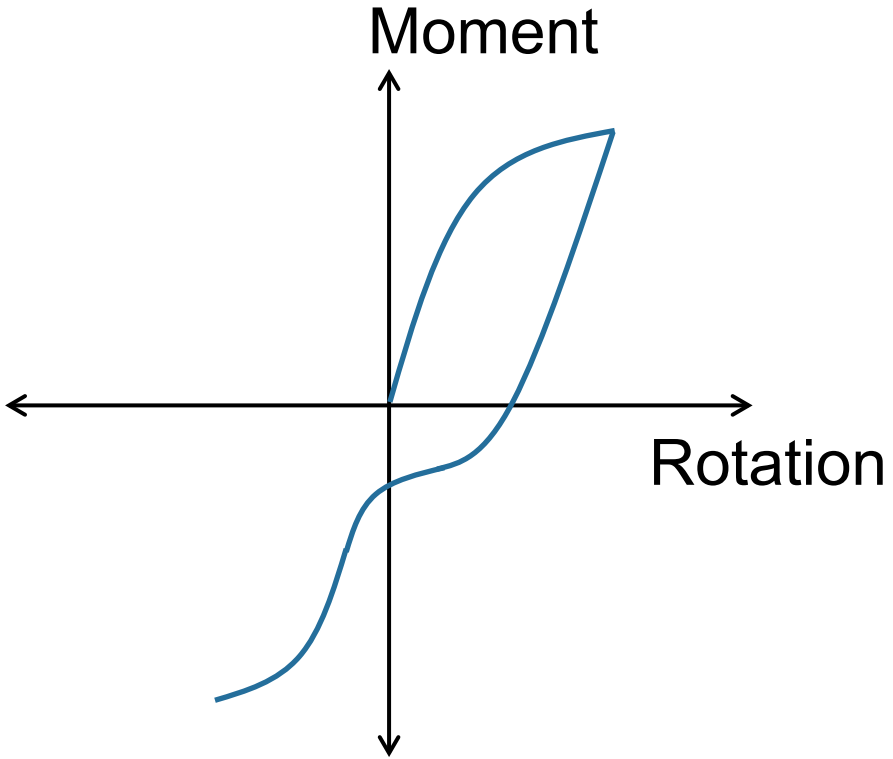
Intended behavior





Intended behavior





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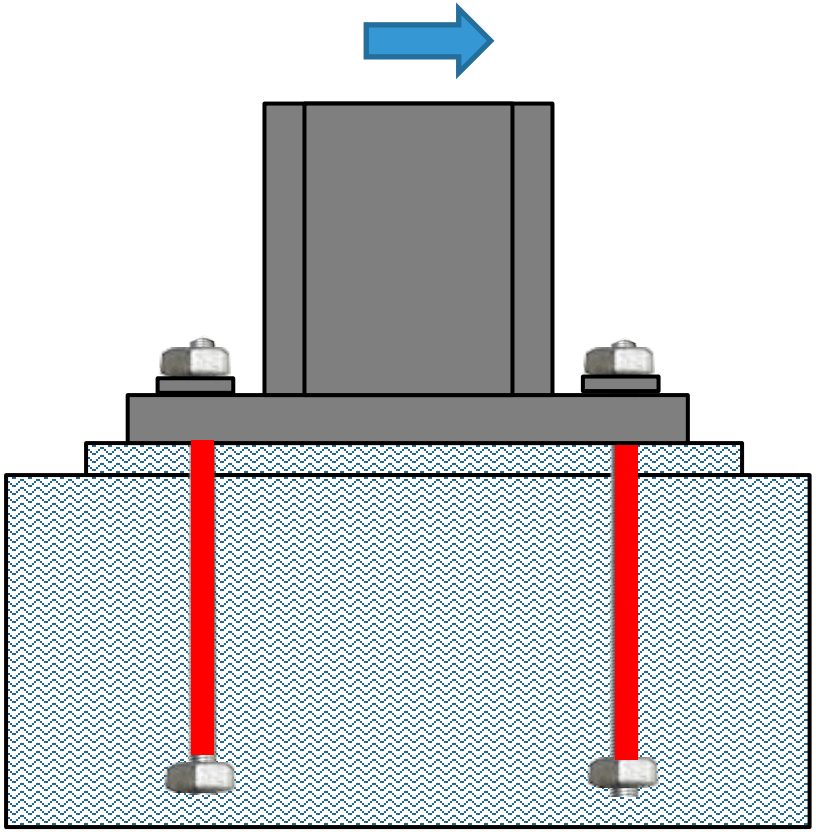

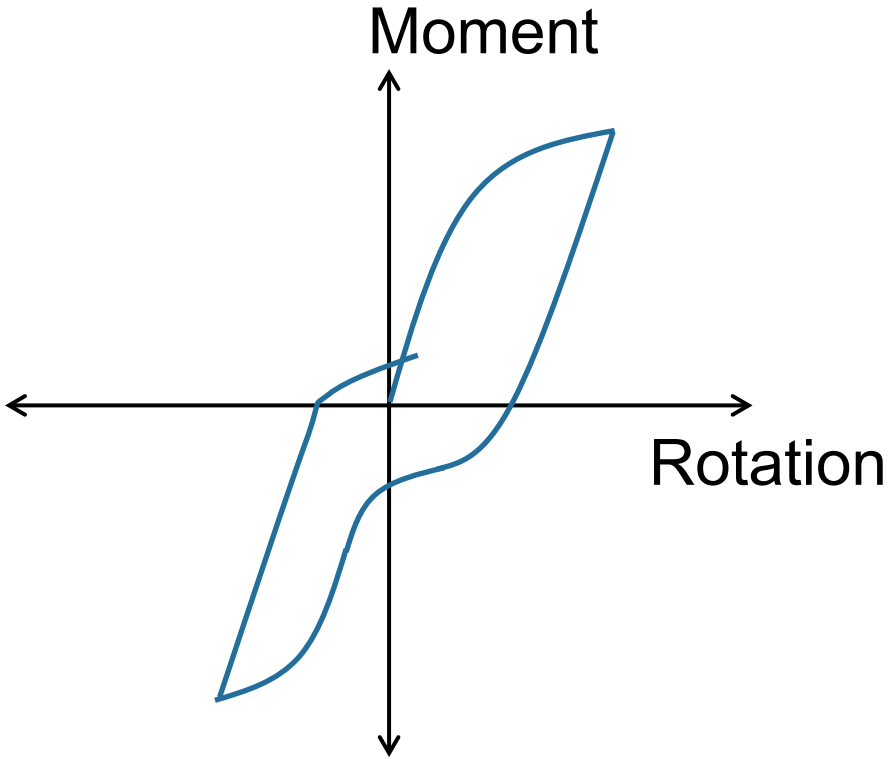

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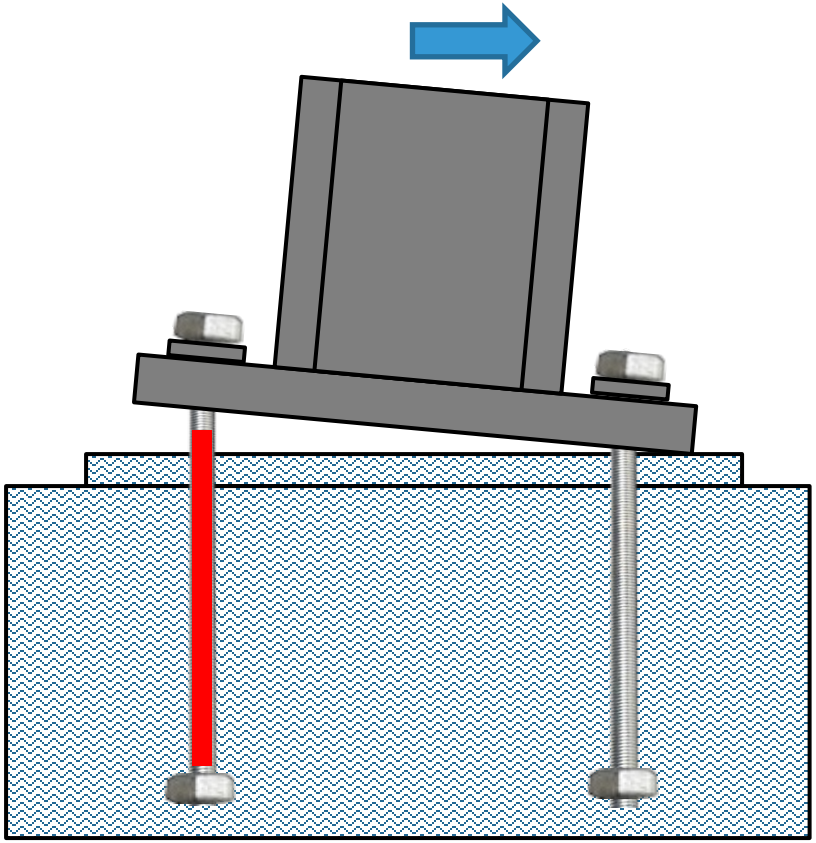
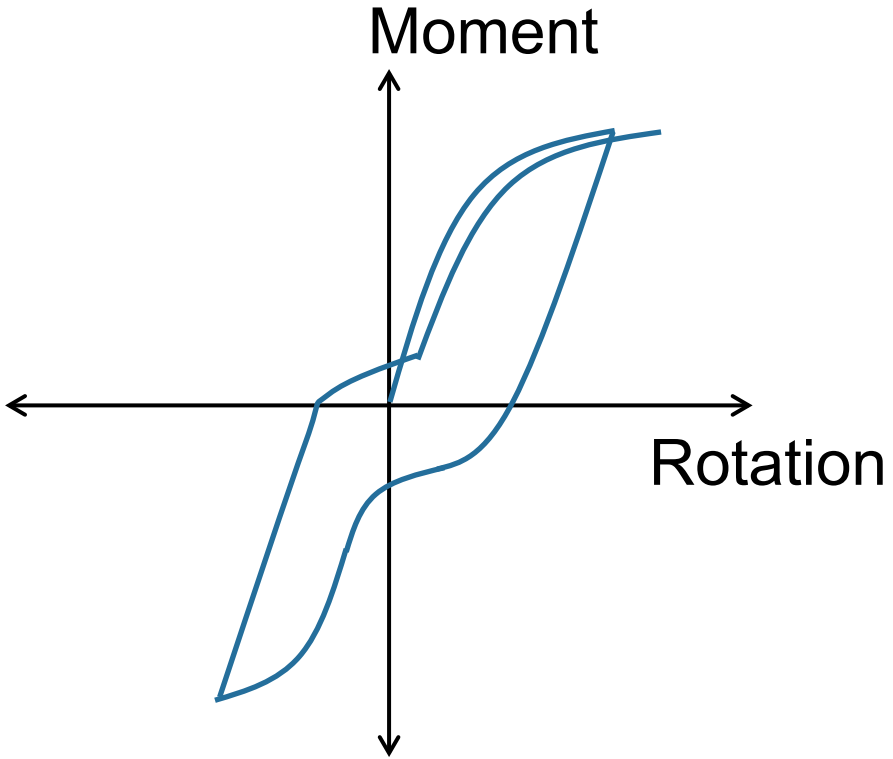
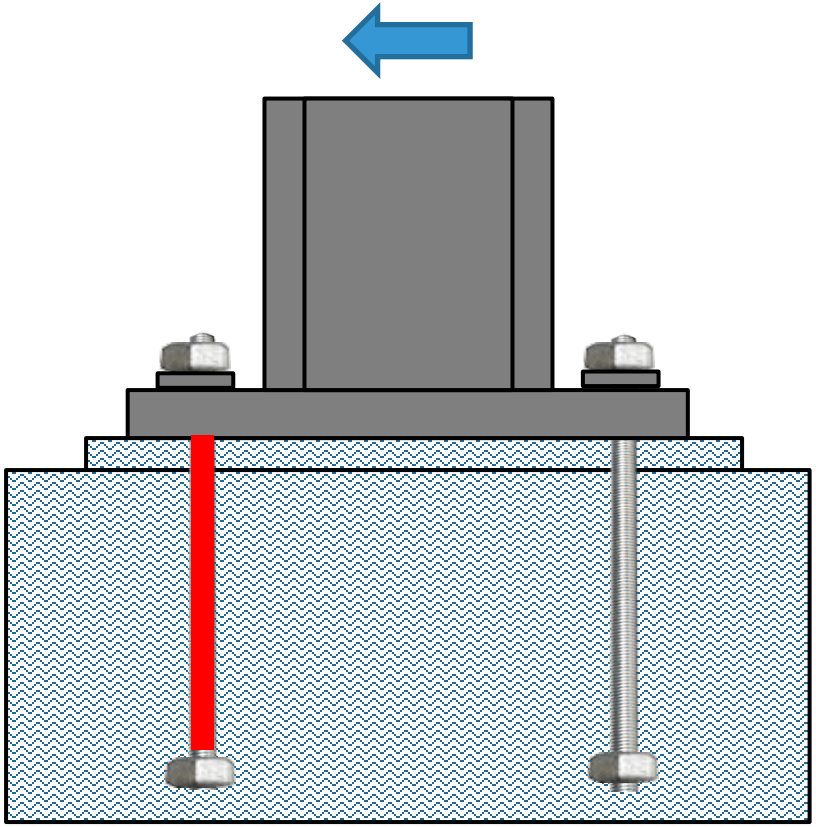
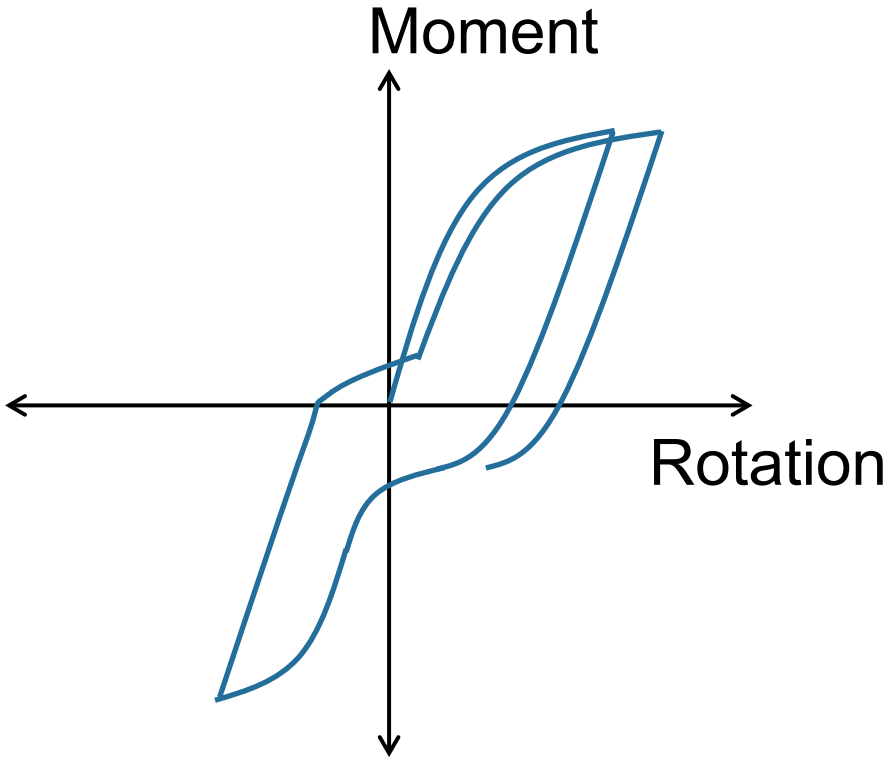


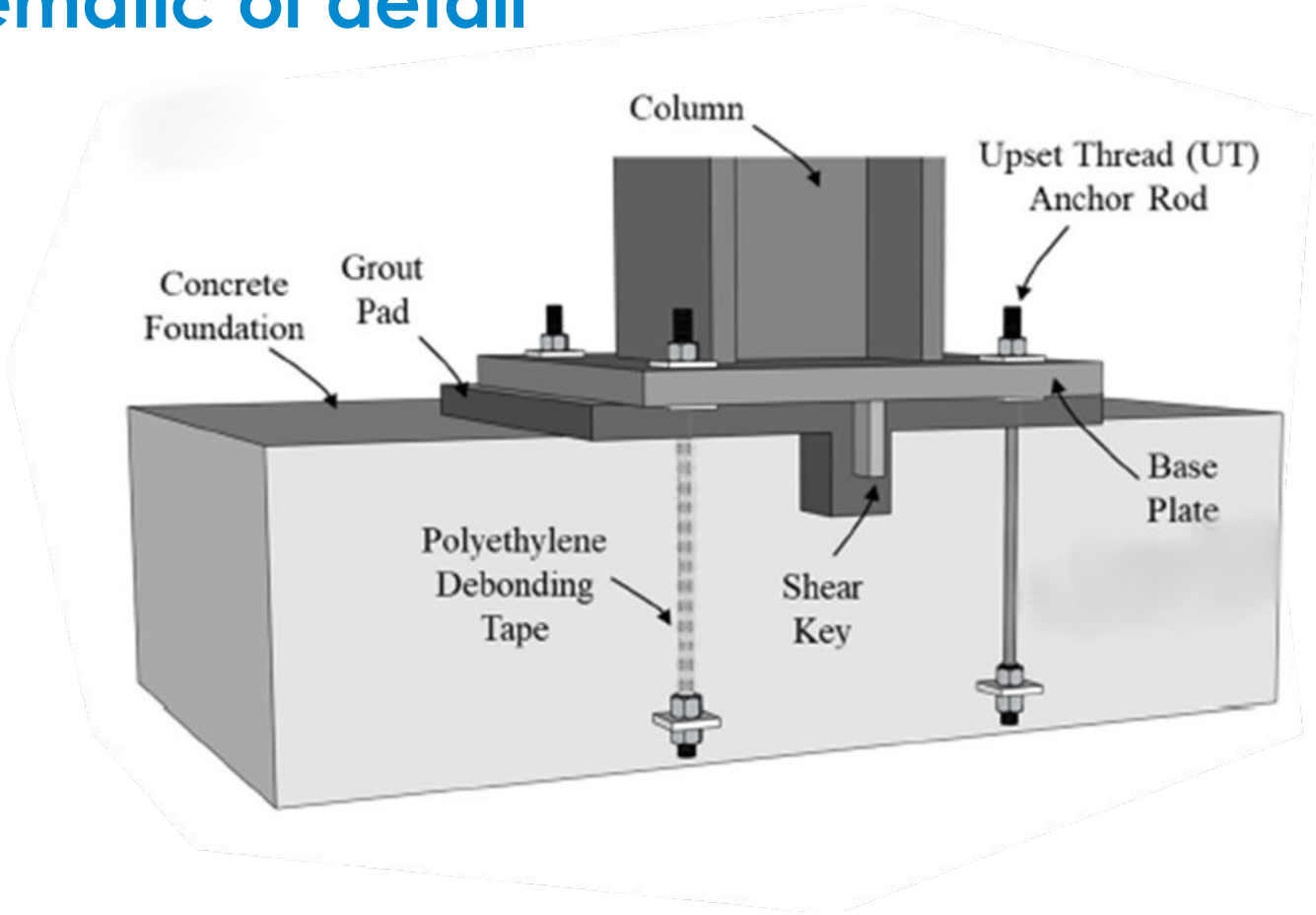


Intended behavior



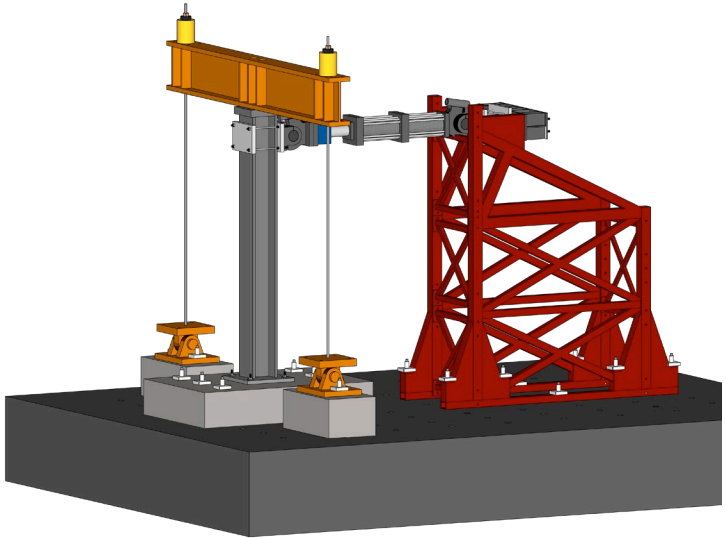


Schematic of detail



Large scale tests and performance

Test #	Base Plate size [in]	Anchor Grade	Anchor Dia [in]	Axial Load [kip]
1	30 x 30 x 2	55	0.75	120 (C)
2			1.00	120 (C)
3		105		120 (C)
4				0



Large scale tests and performance

Test #	Base Plate size [in]	Anchor Grade	Anchor Dia [in]	Axial Load [kip]
1	30 x 30 x 2	55	0.75	120 (C)
2			1.00	120 (C)
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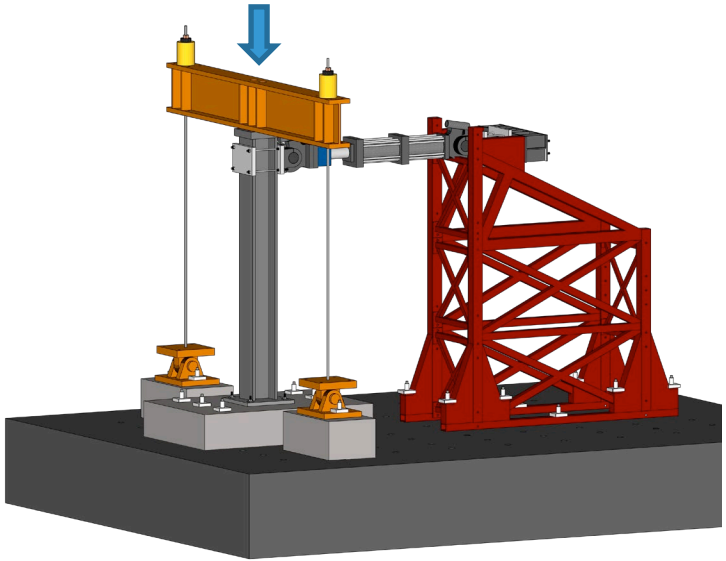
4				0



Large scale tests and performance

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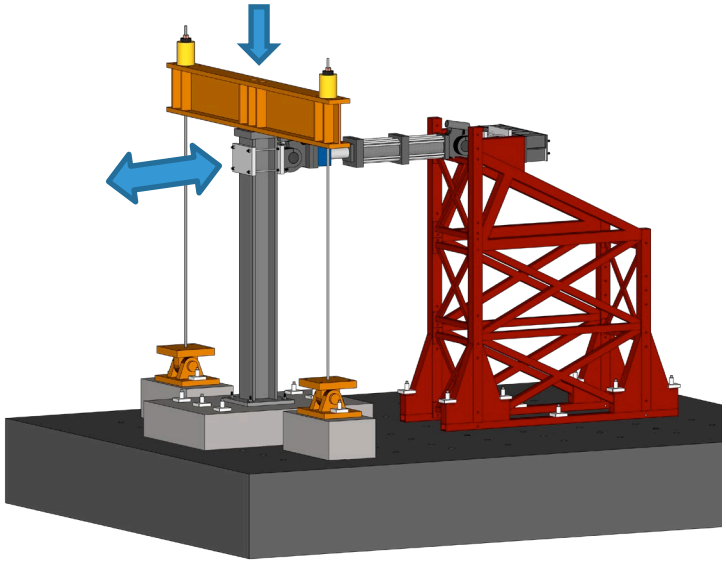
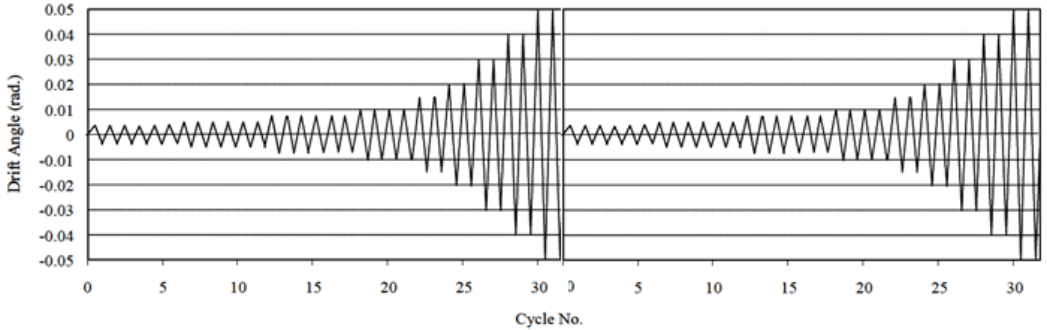


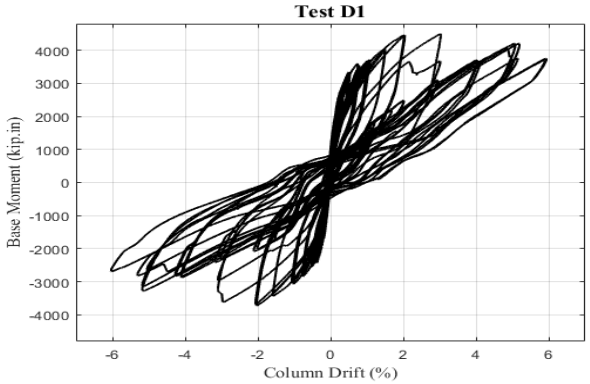


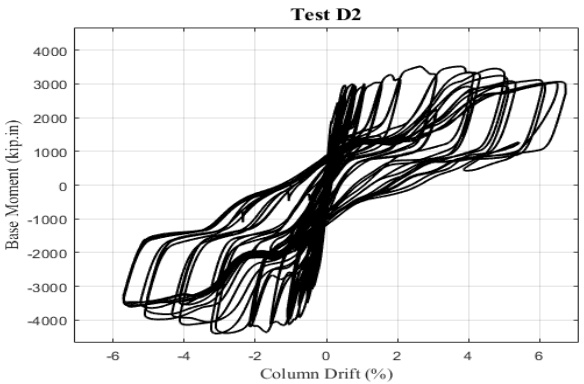
ATC-SAC Protocol applied twice followed by 6.5% cycles

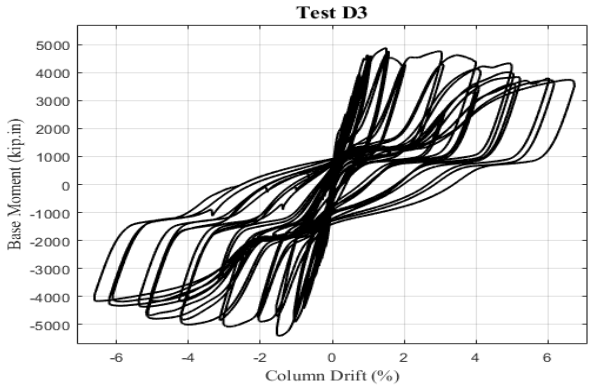
Results

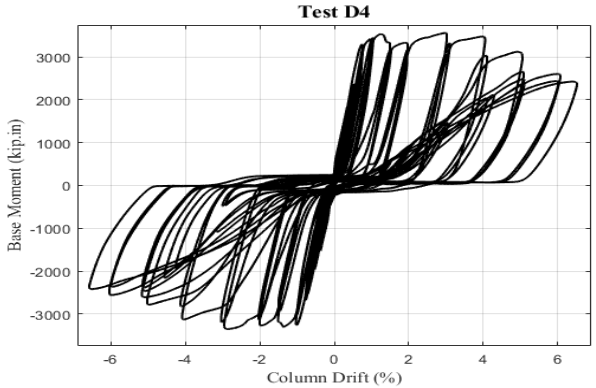
All specimens survived back to back applications of SAC protocol (to 5%) and additional cycles to 6.5% with no rod fracture

Results



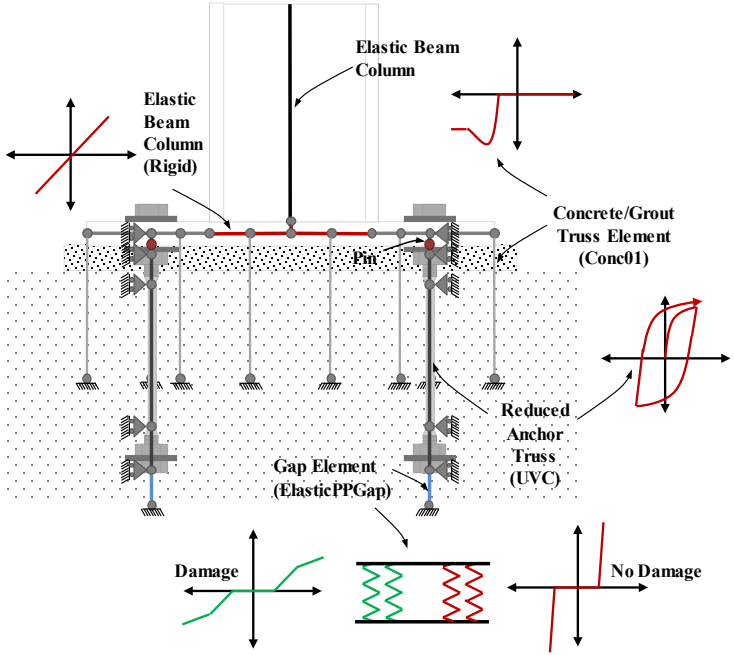


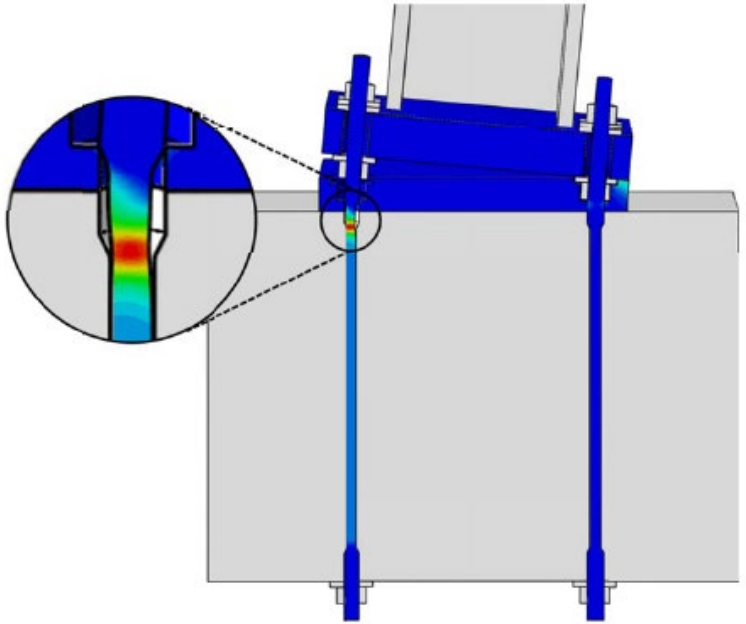




Predominant damage – grout crushing

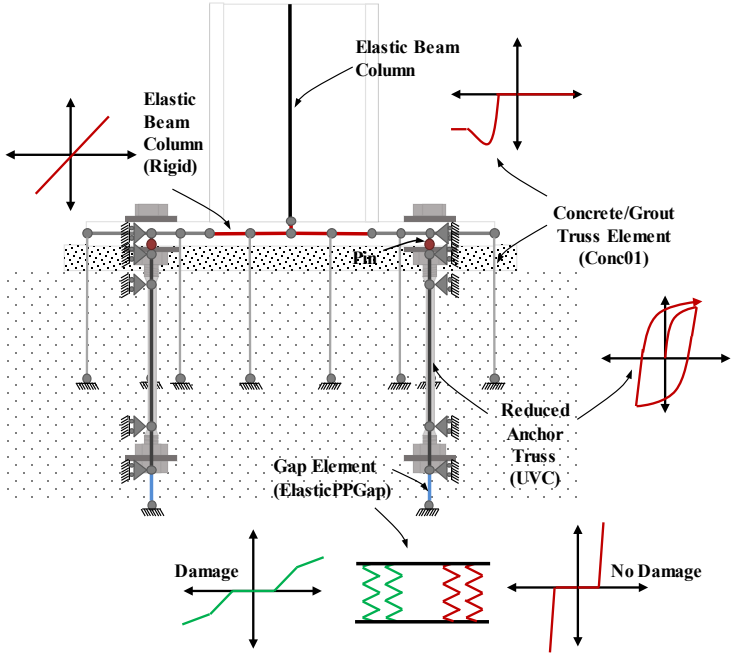
Generalization using material testing, FEM, and line-based simulations

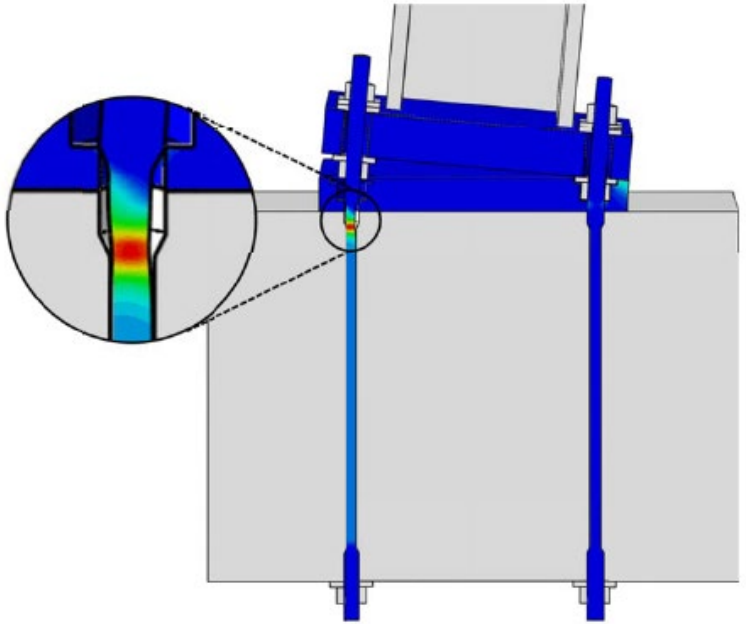




Simulation of Necking, Ultra Low Cycle Fatigue, Bending

Generalization using material testing, FEM, and line-based simulations

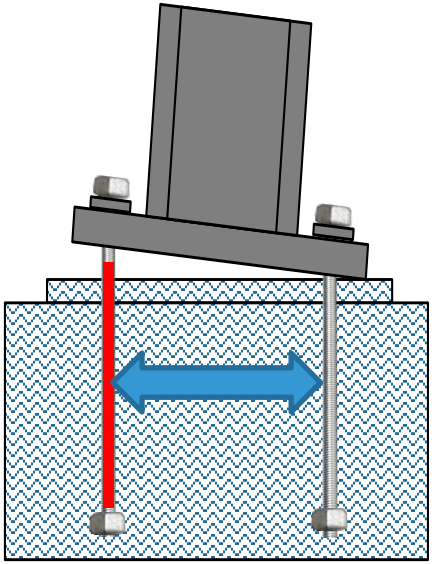




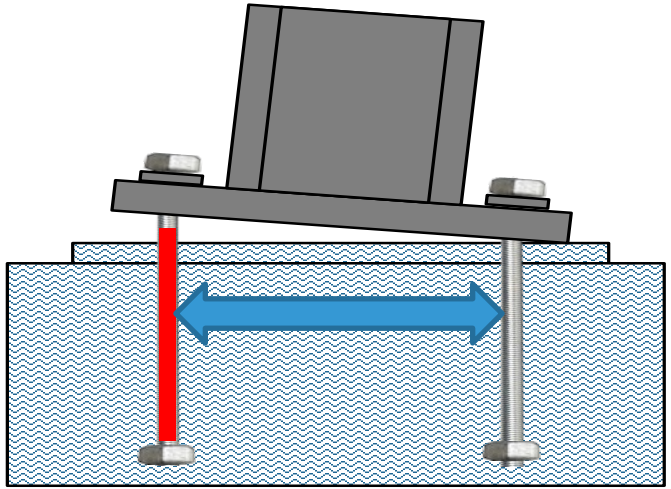
~60 parametric simulations with variations in plate and rod dimensions, rod materials, loading histories etc.

Parametric Simulation – findings

- Behavior appears to hold across a large number of configurations
- Ratio of stretch length to plate length is key

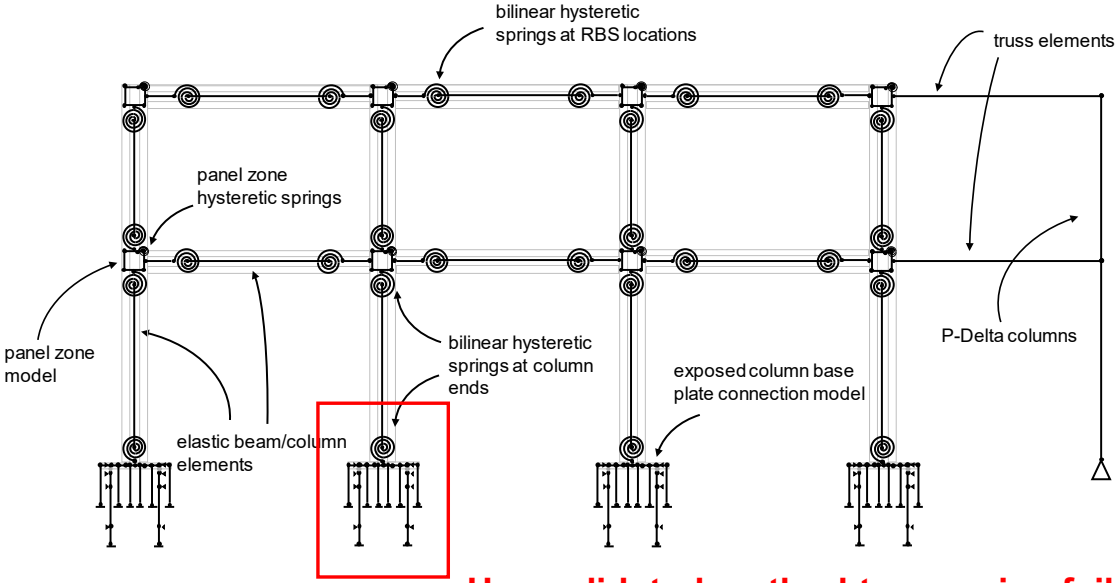


$L_{stretch} > 1/2 \times L_{plate}$



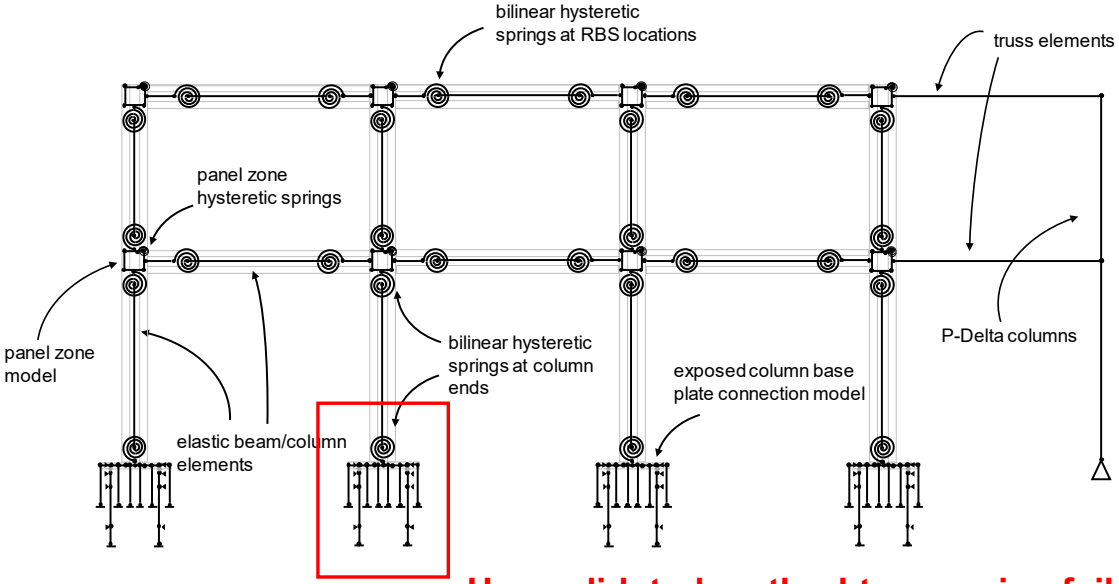
$L_{stretch} < 1/2 \times L_{plate}$

NLTHA Results and summary



Use validated method to examine failure

NLTHA Results and summary

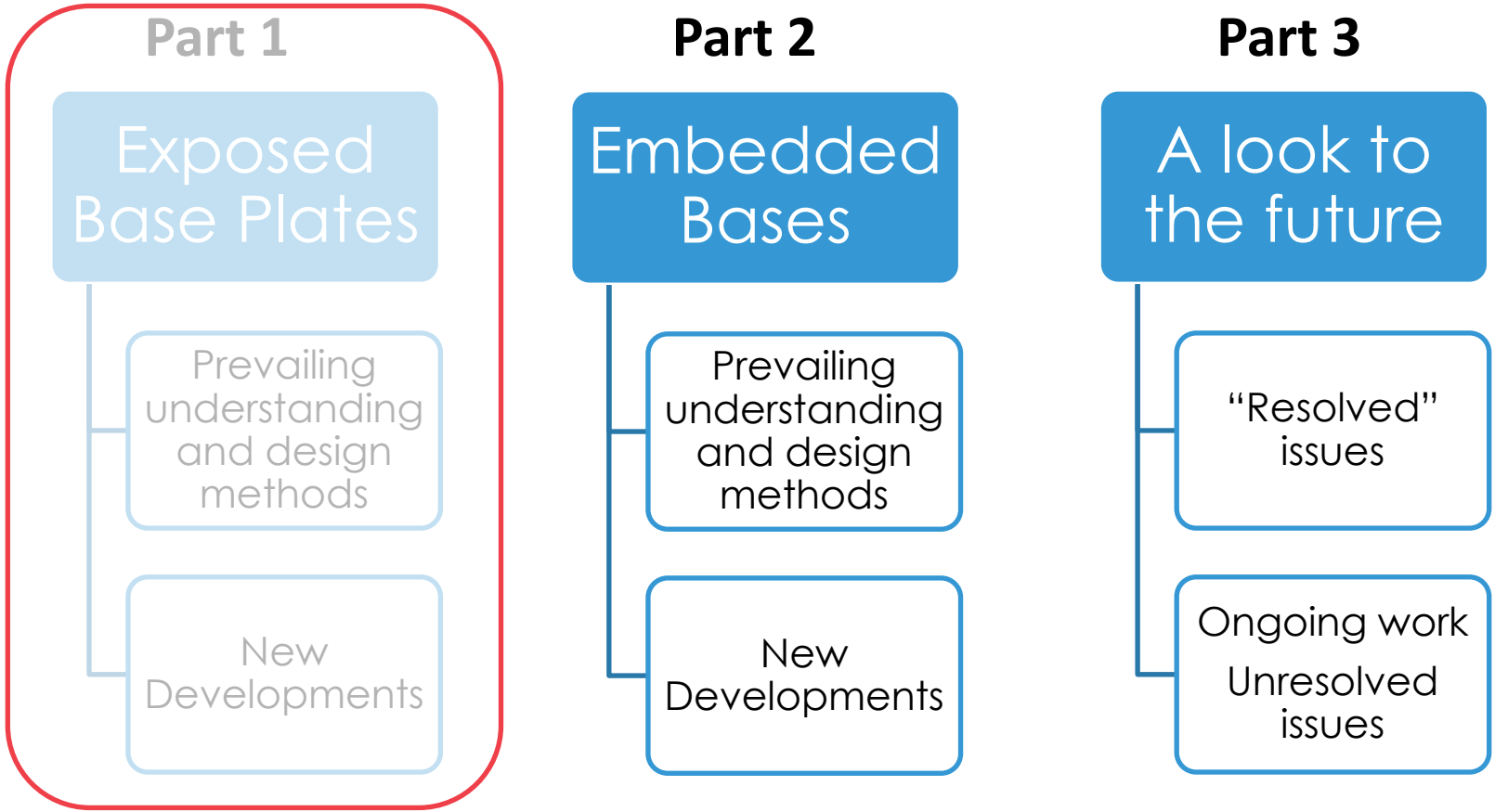


Use validated method to examine failure

- Upset Thread detail with $L_{stretch}$ > 1/2 X L_{plate}
- Ω_0 based design of connection

Excellent performance

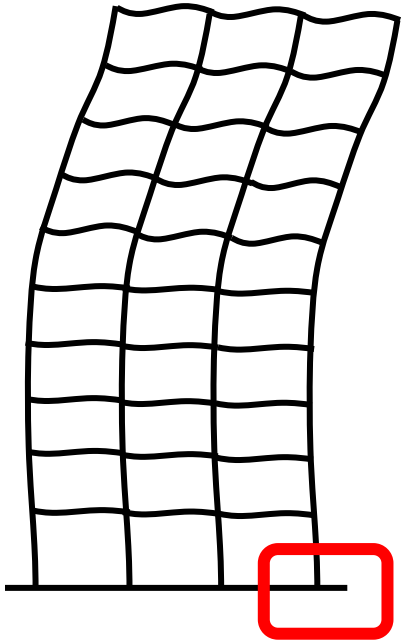
Organization

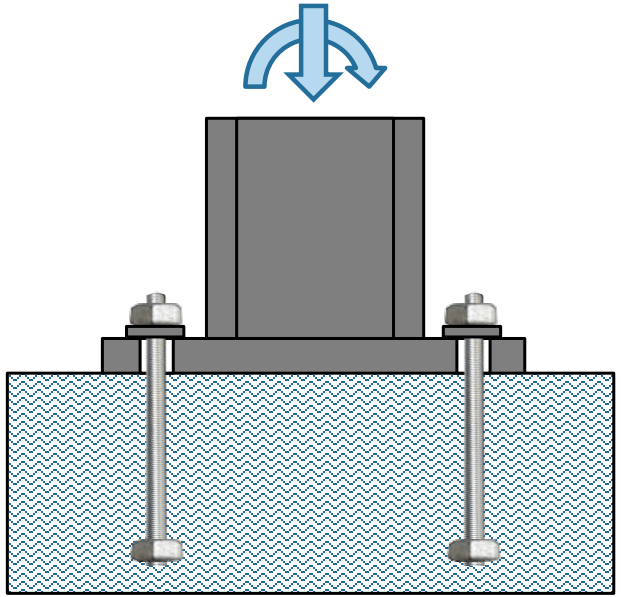


Part 2 – Embedded Base Connections

Embedded Bases

- Prevailing understanding and design methods
- New Developments



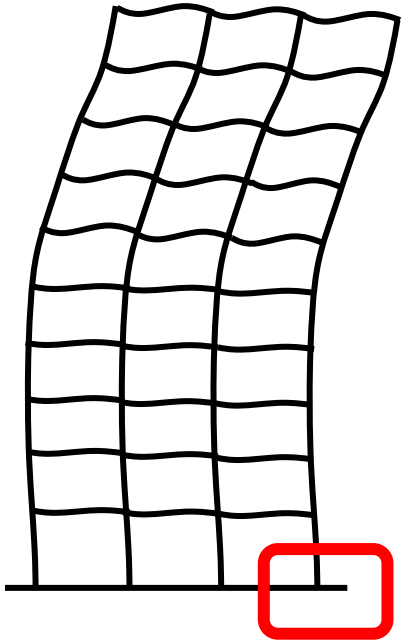


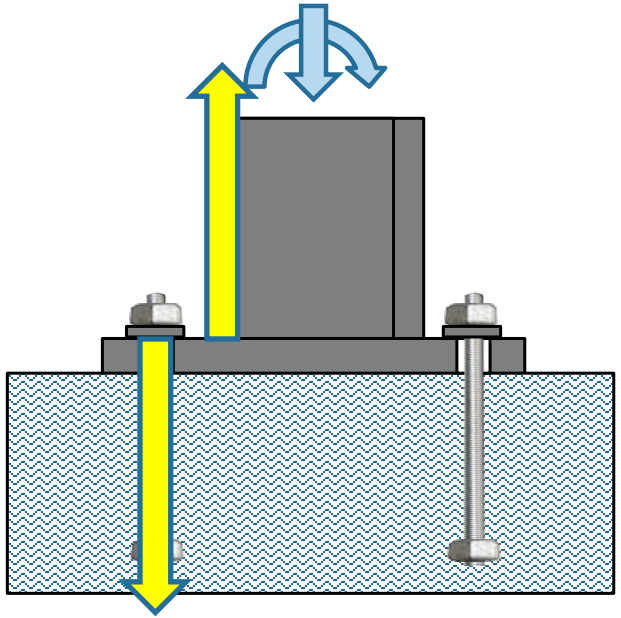
High rise buildings
Large column moments

Part 2 – Embedded Base Connections

Embedded Bases

- Prevailing understanding and design methods
- New Developments





Developing column capacity is challenging

Part 2 – Embedded Base Connections

- Embedded Bases
  - Prevailing understanding and design methods
  - New Developments

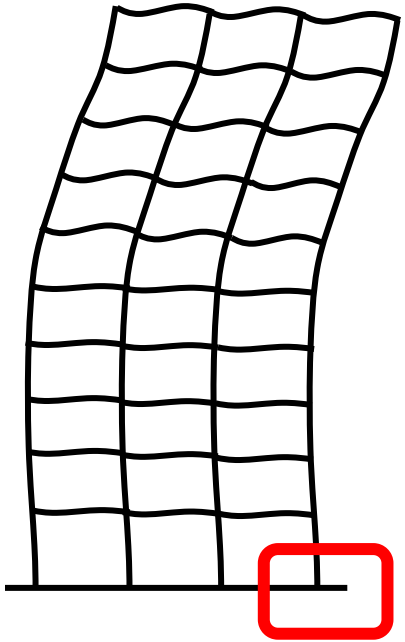


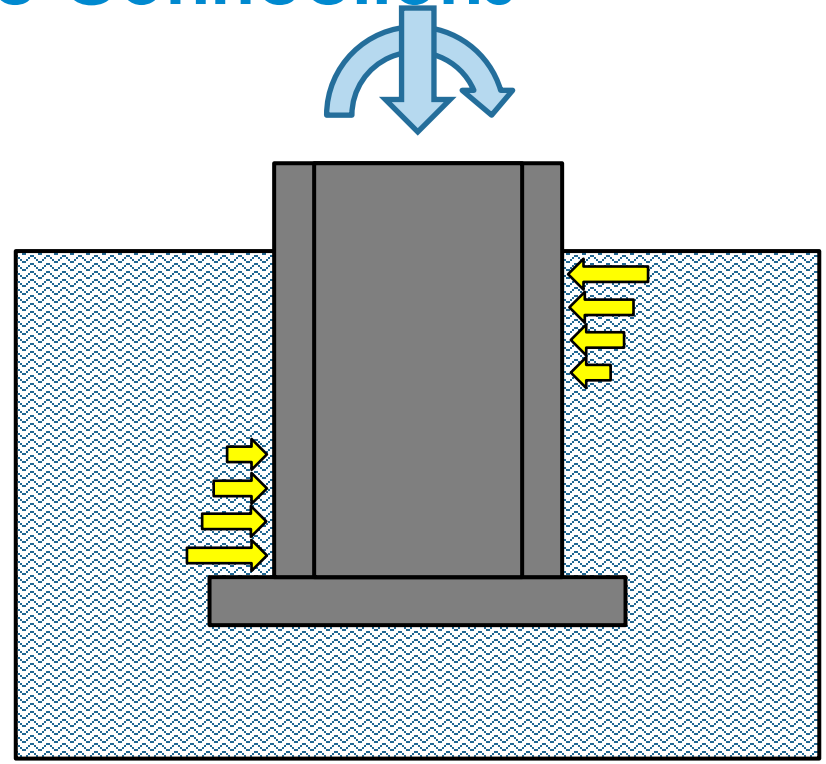
Photo credit: Josh Buckholt and Mahmoud Maamouri, CSD Engineers

Developing column capacity is challenging

Part 2 – Embedded Base Connections

Embedded Bases

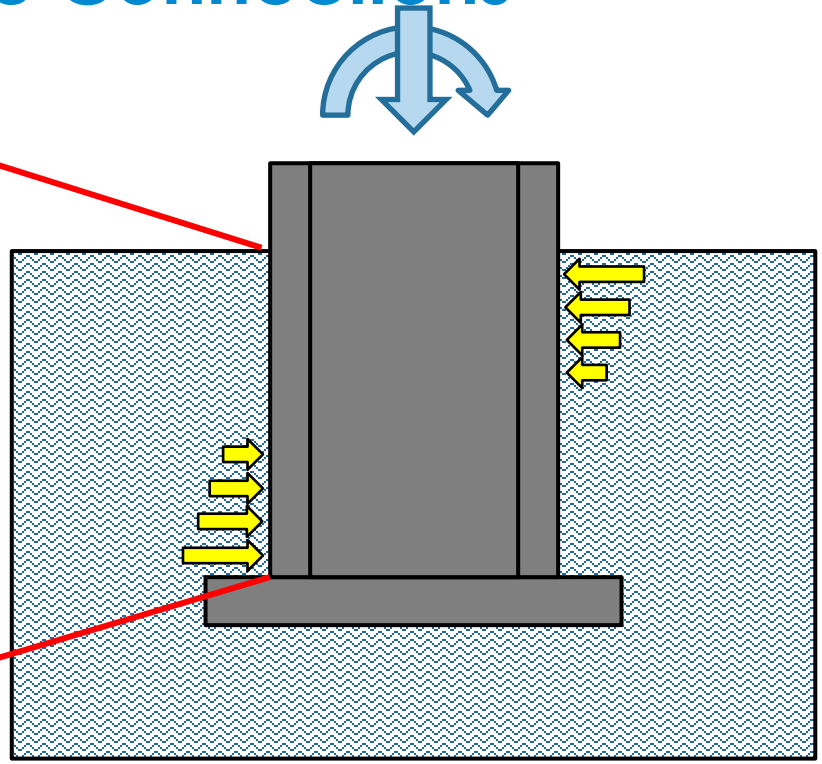
- Prevailing understanding and design methods
- New Developments



Resistance through concrete bearing

Part 2 – Embedded Base Connections

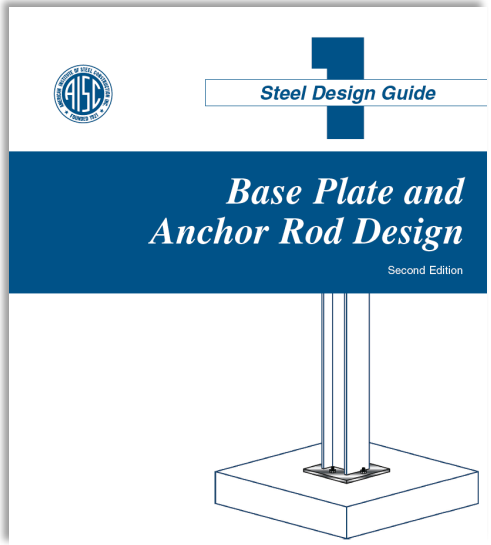
Photo credit: Nabih Youssef, Simpson Gumpertz and Heger

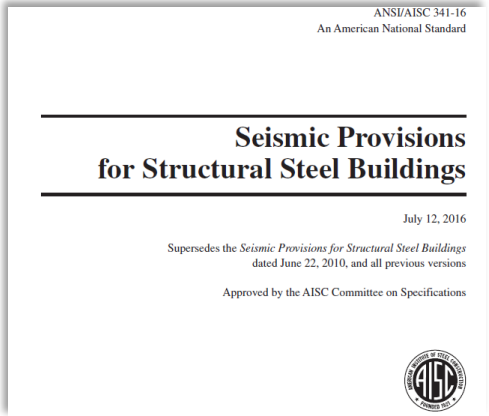


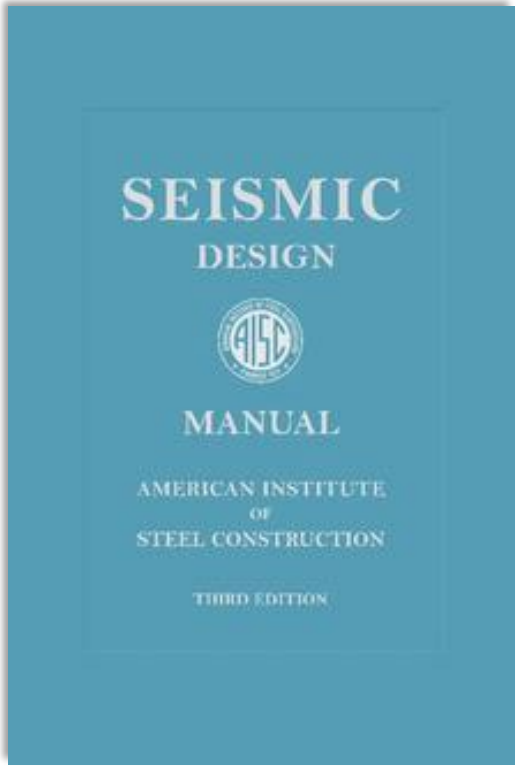
Resistance through concrete bearing

Overview

- Embedded Bases
  - Prevailing understanding and design methods
  - New Developments







Takeaways from Design Documents

- AISC 341 and Design Guide One identify embedded details
- AISC 341 – Commentary points to similar details
- SSDM uses coupling beam analogy

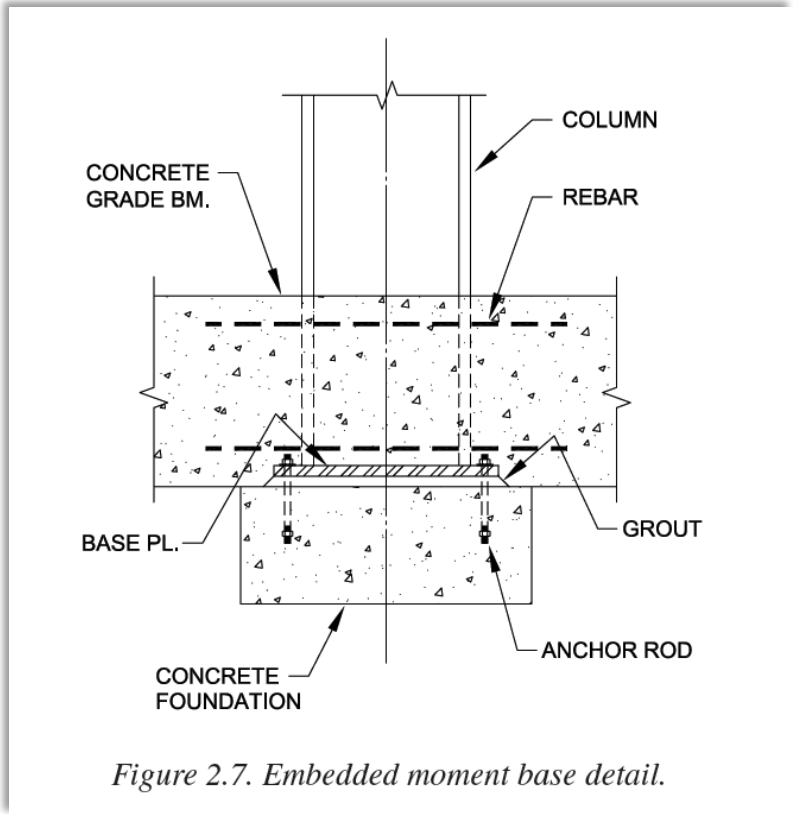


Figure 2.7. Embedded moment base detail.

Takeaways from Design Documents

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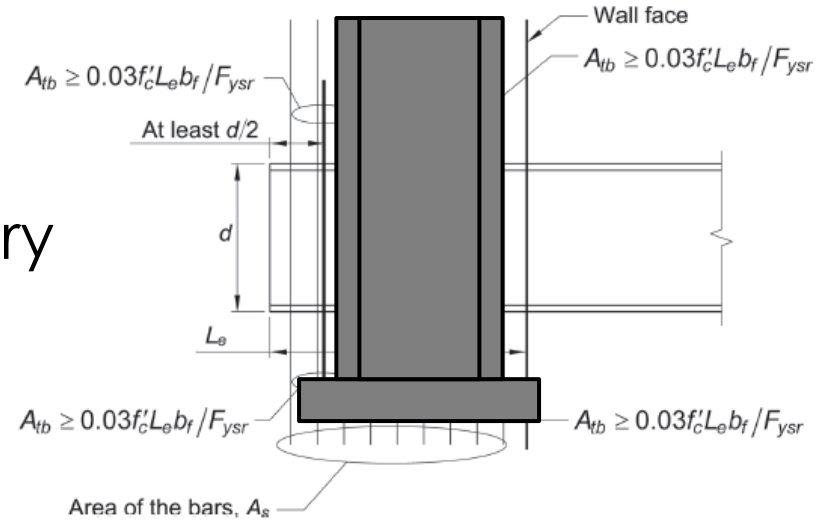
- AISC 341 – Commentary points to similar details
- SSDM uses coupling beam analogy



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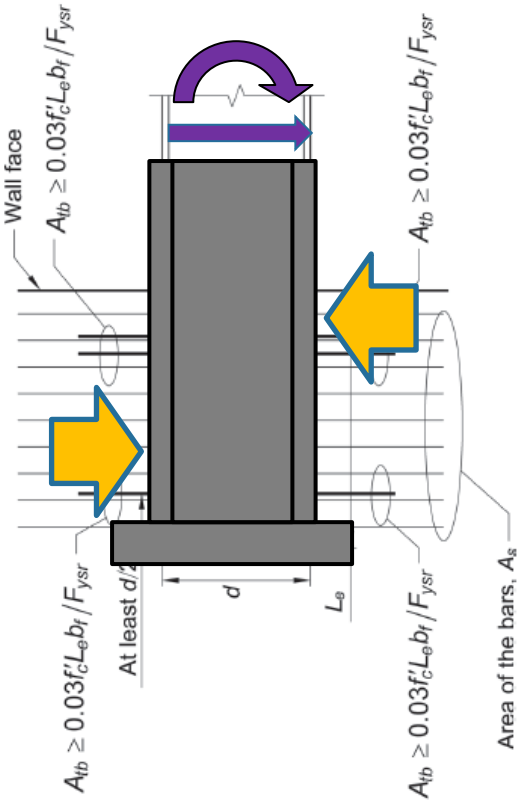
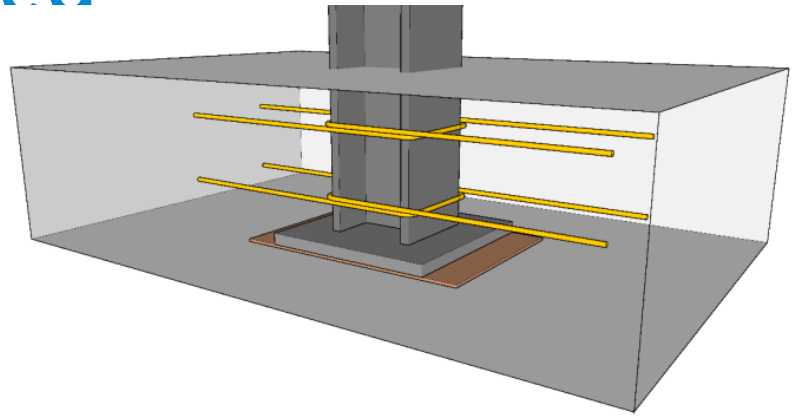


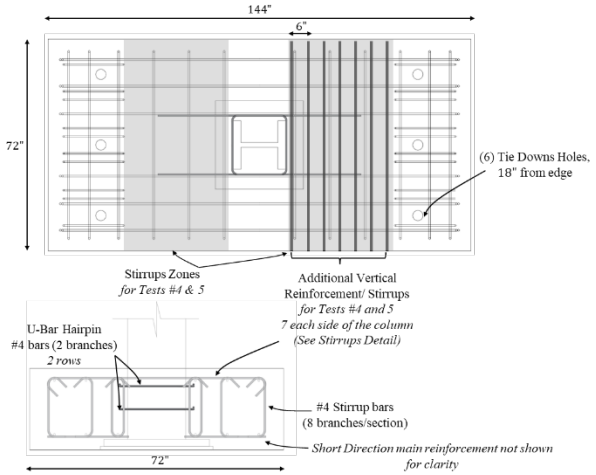
Research in the last 15 years

- 10 Experiments
- Finite element simulations
- Strength and stiffness models

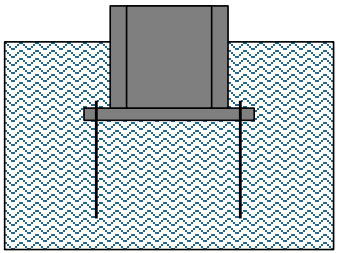
Various variables investigated

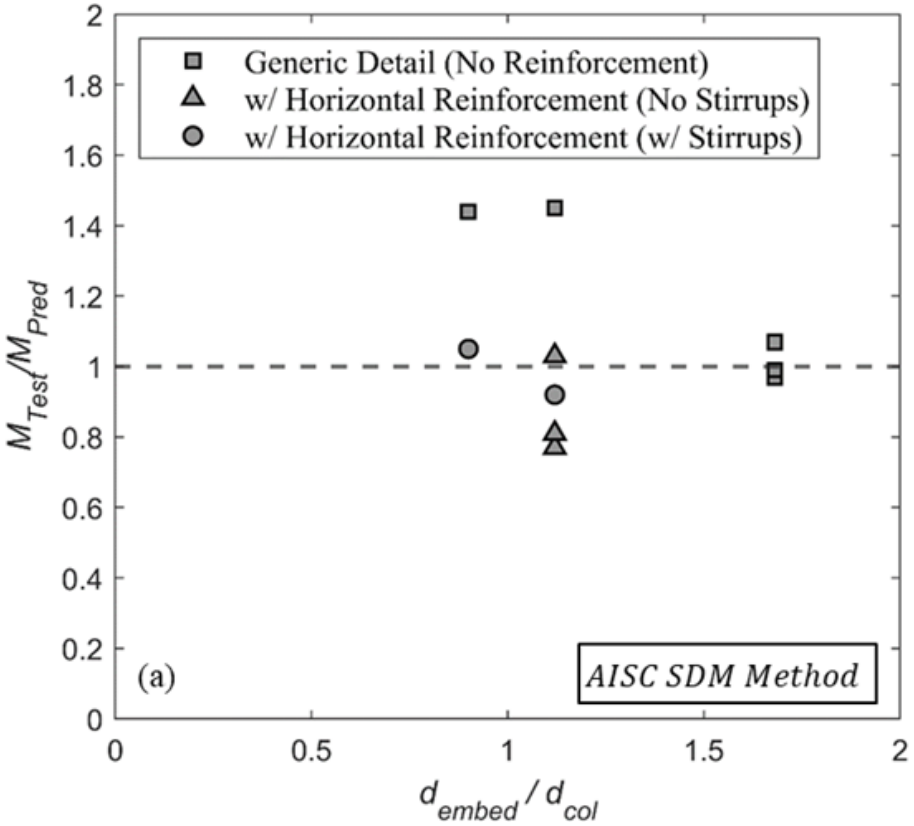
- Embedment depth
- Axial compression
- Column size
- Reinforcement (horizontal and vertical)

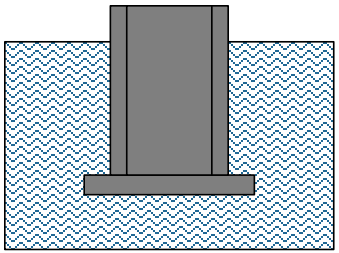




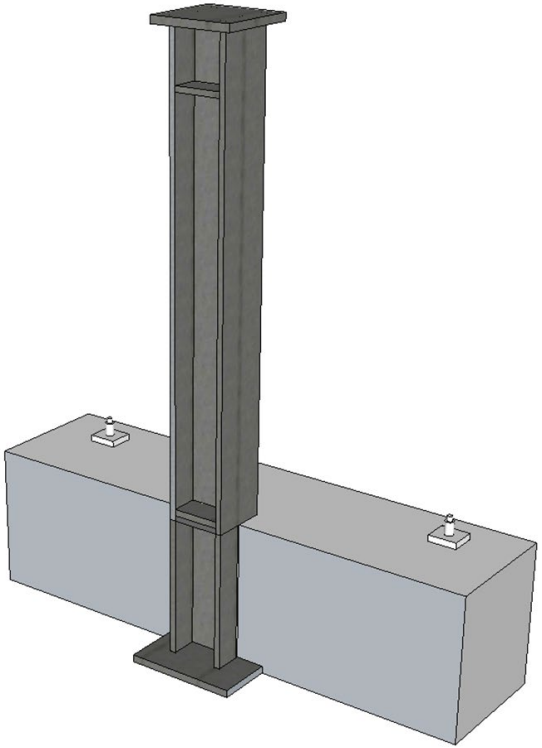
Coupling beam approach applied to test data







Embedded base connections are NOT coupling beams



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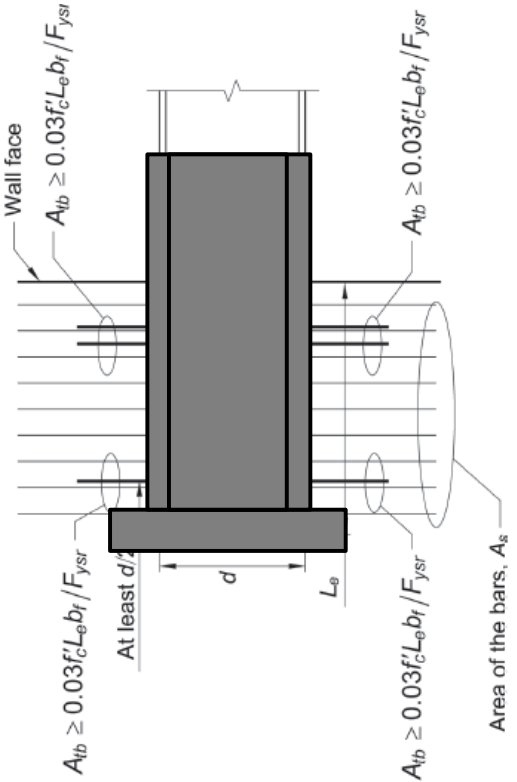
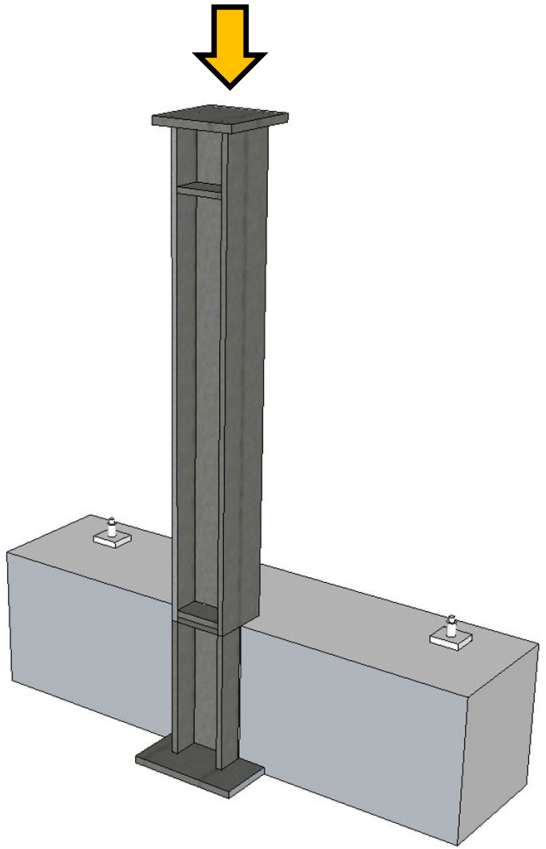
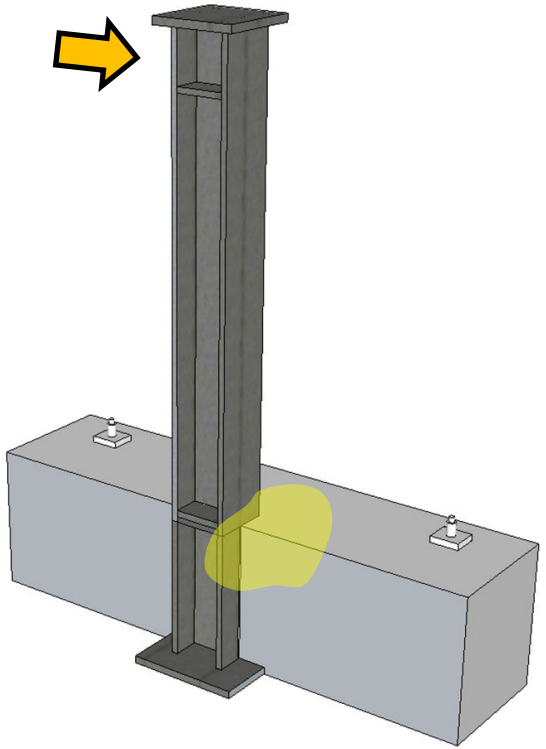


Embedded base connections are NOT coupling beams



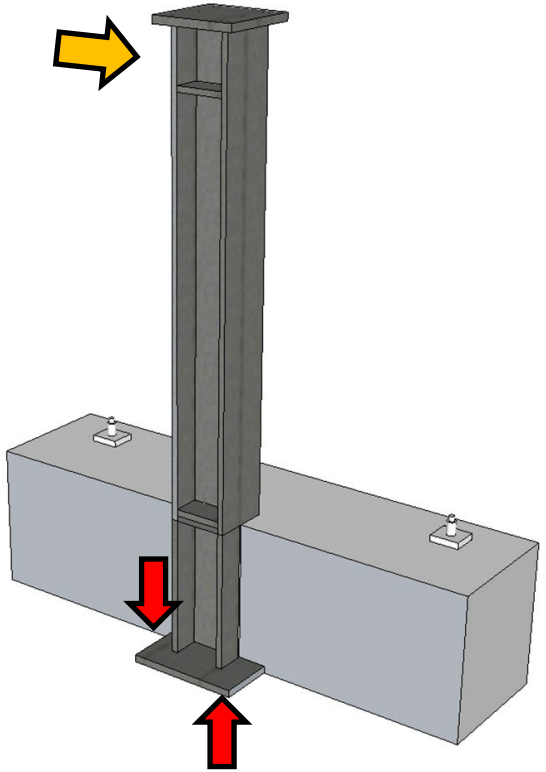
- Effect of axial force
- Additional confinement around column flanges
- Fixity and strength due to vertical bearing

Embedded base connections are NOT coupling beams



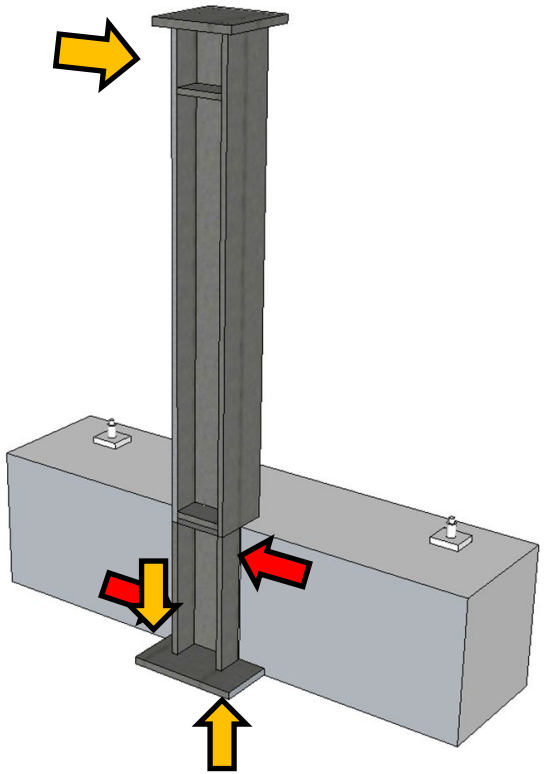
- Effect of axial force
- Additional confinement around column flanges
- Fixity and strength due to vertical bearing

Embedded base connections are NOT coupling beams



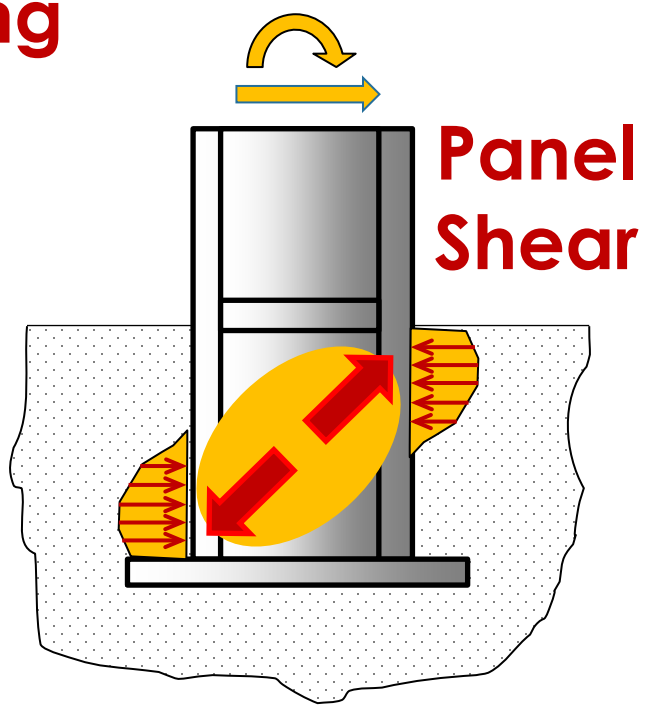
- Effect of axial force
- Additional confinement around column flanges
- Fixity and strength due to vertical bearing

New model for embedded base connections

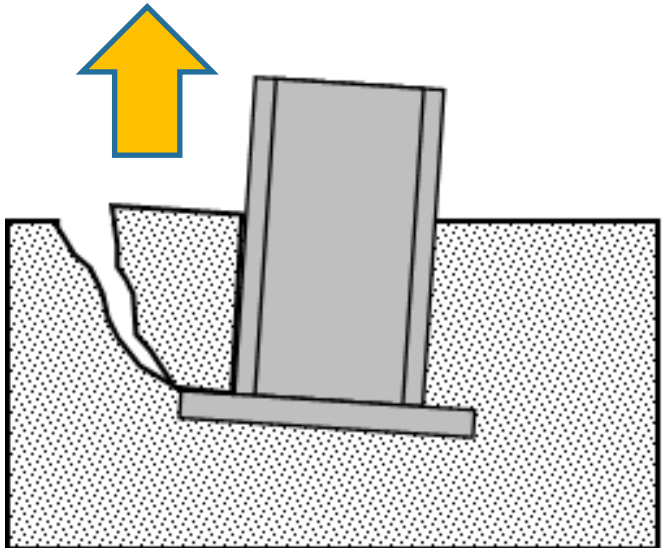


- Horizontal bearing against column flanges
- Vertical bearing against embedded plate
- Consideration of interactions and failure modes

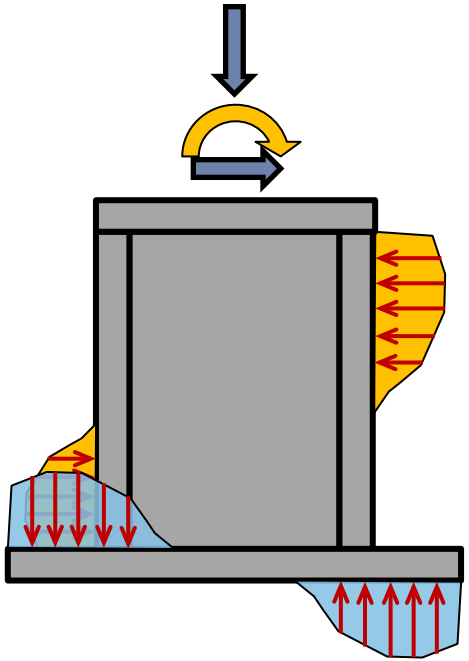
Horizontal Bearing and panel shear – similar to coupling beams



Vertical bearing



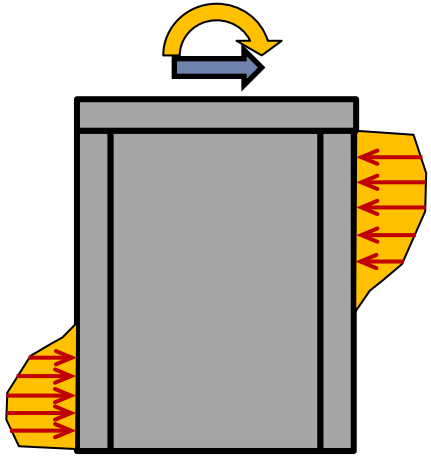
Strength Model – considering both mechanisms



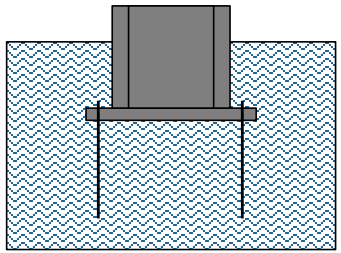
- Idealization of stress blocks
- Consideration of failure modes in each direction
- Consideration of reinforcement patterns

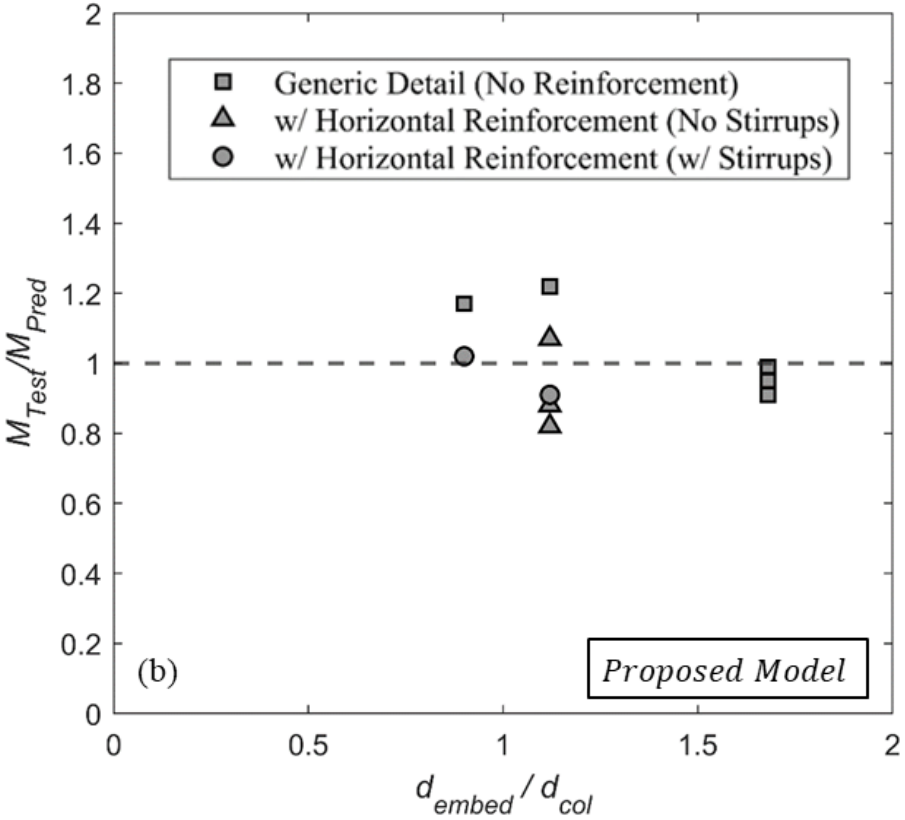
Strength Model

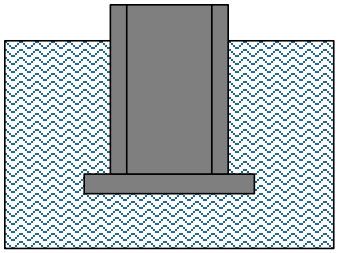
Consideration of failure modes in each direction



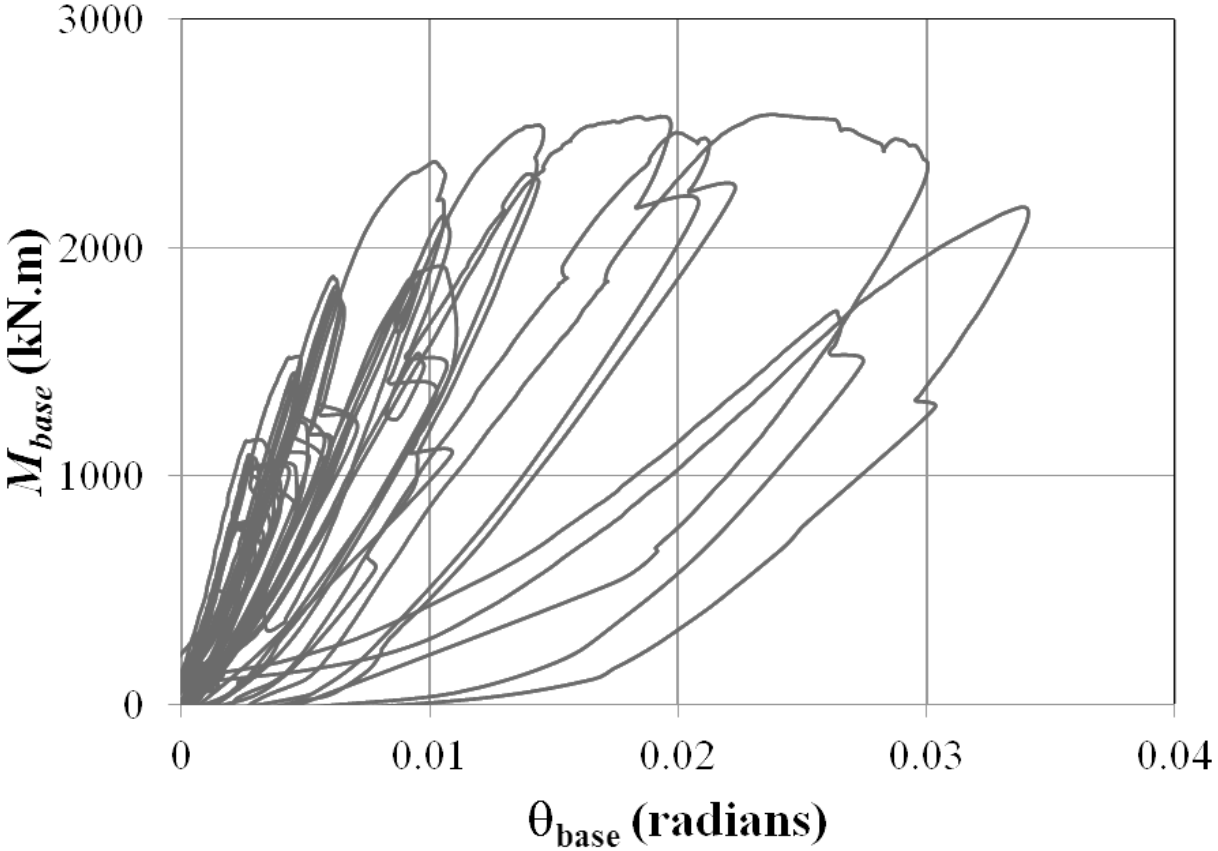
Improved models for embedded bases



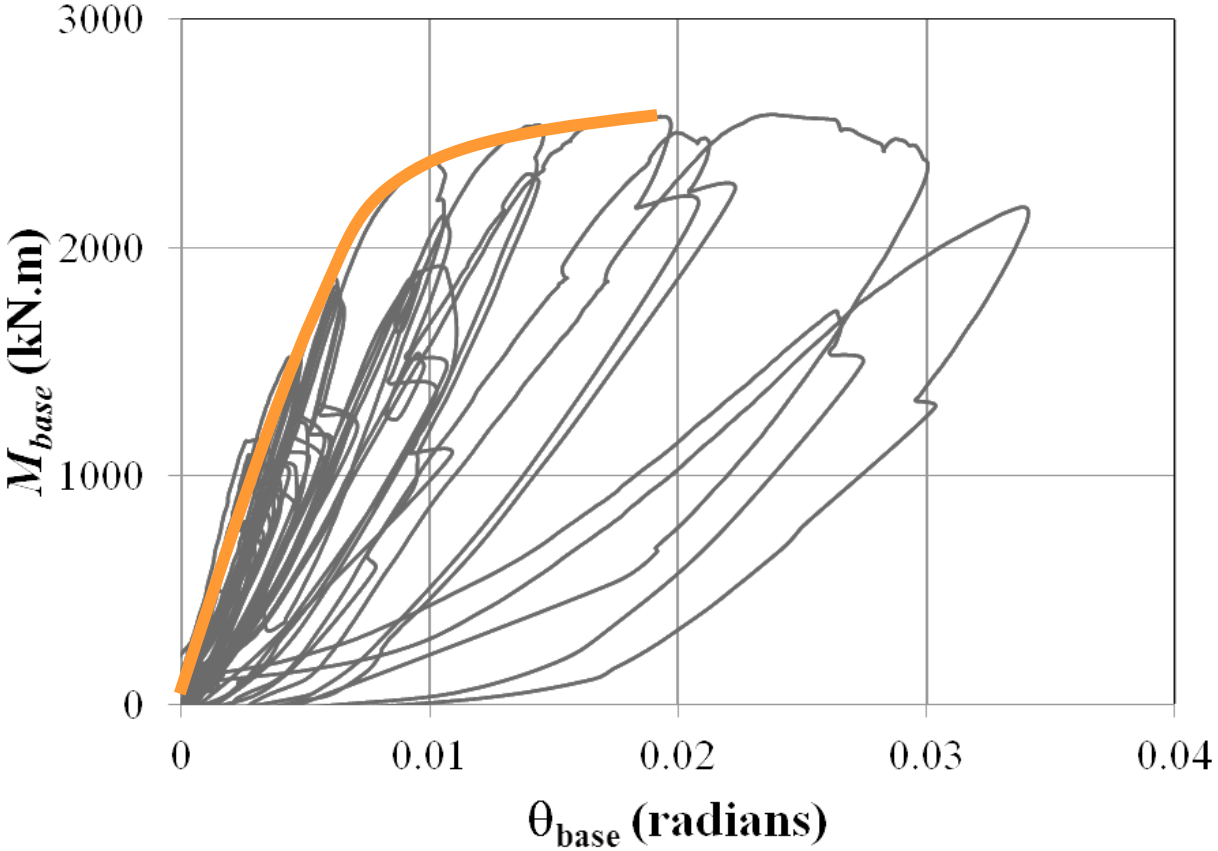




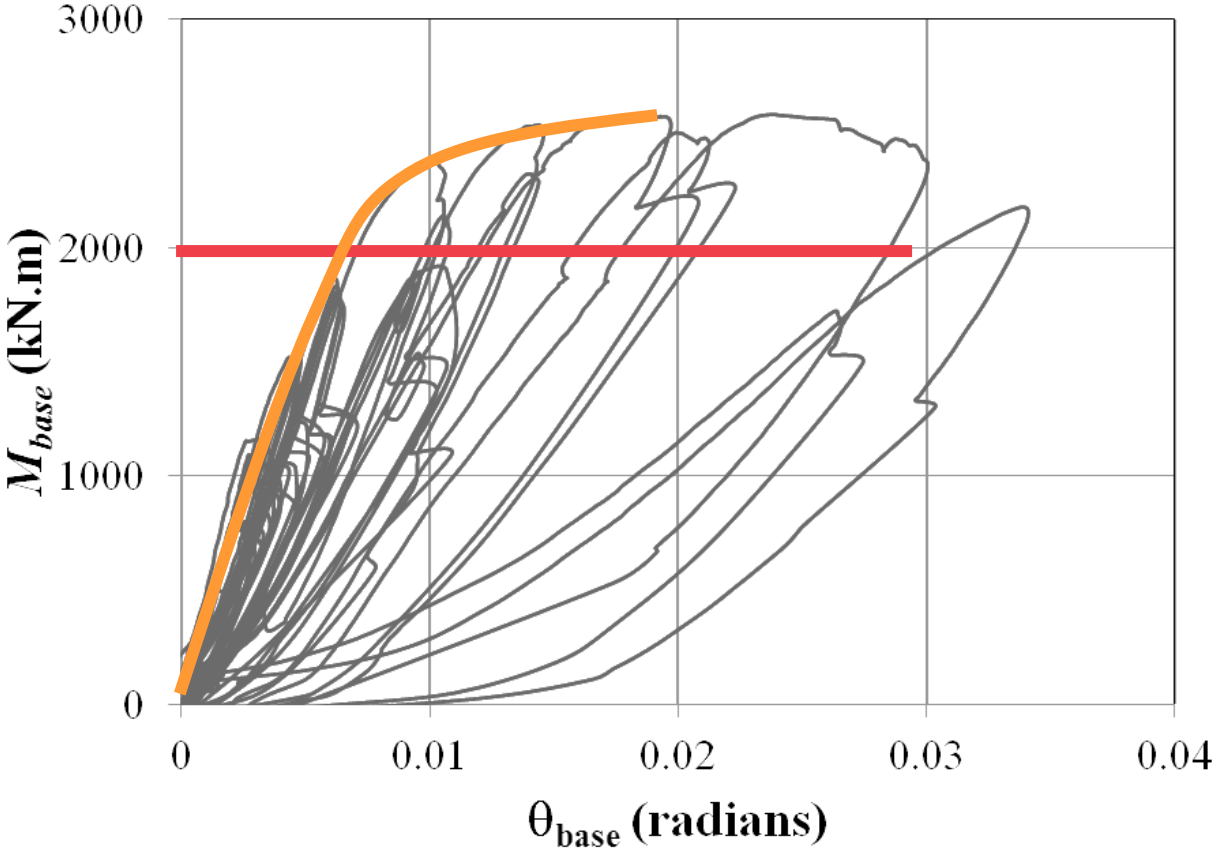
Rotational stiffness of embedded bases



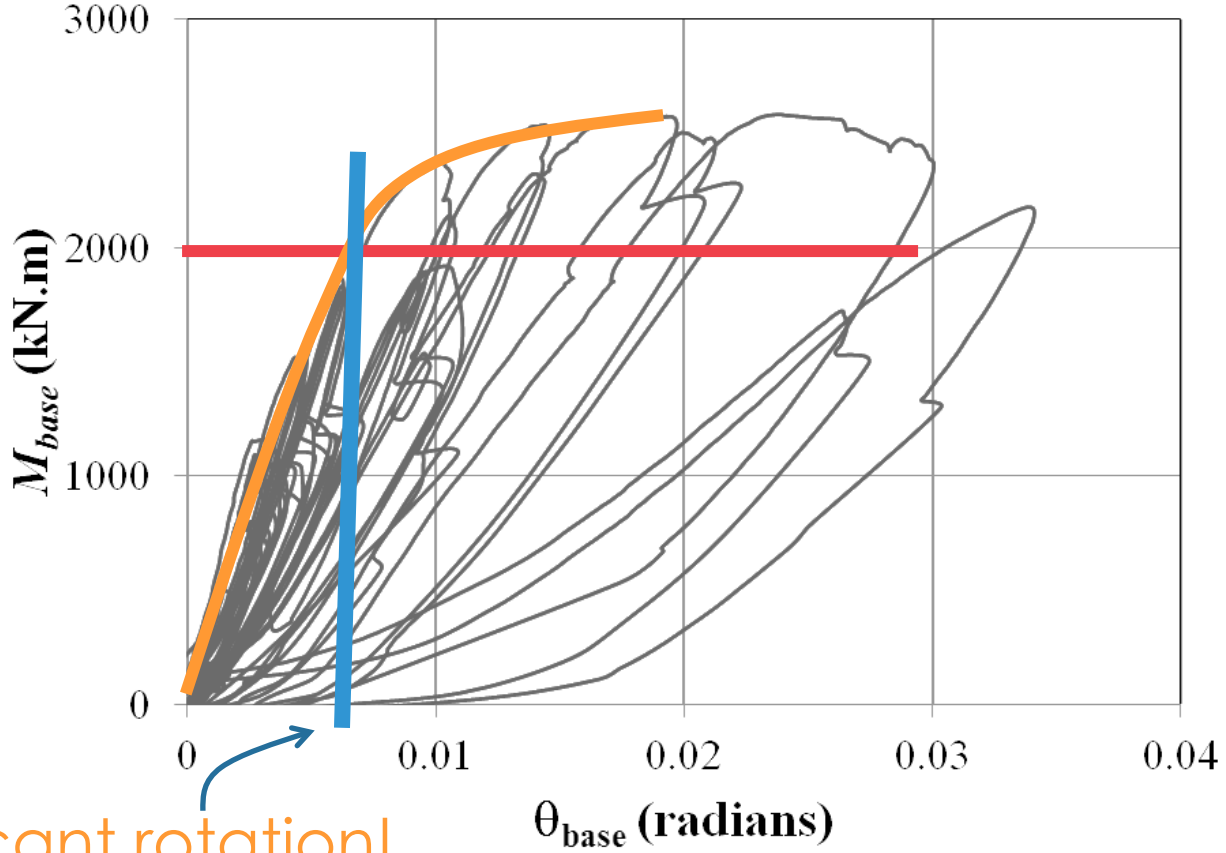
Rotational stiffness of embedded bases



Rotational stiffness of embedded bases



Rotational stiffness of embedded bases

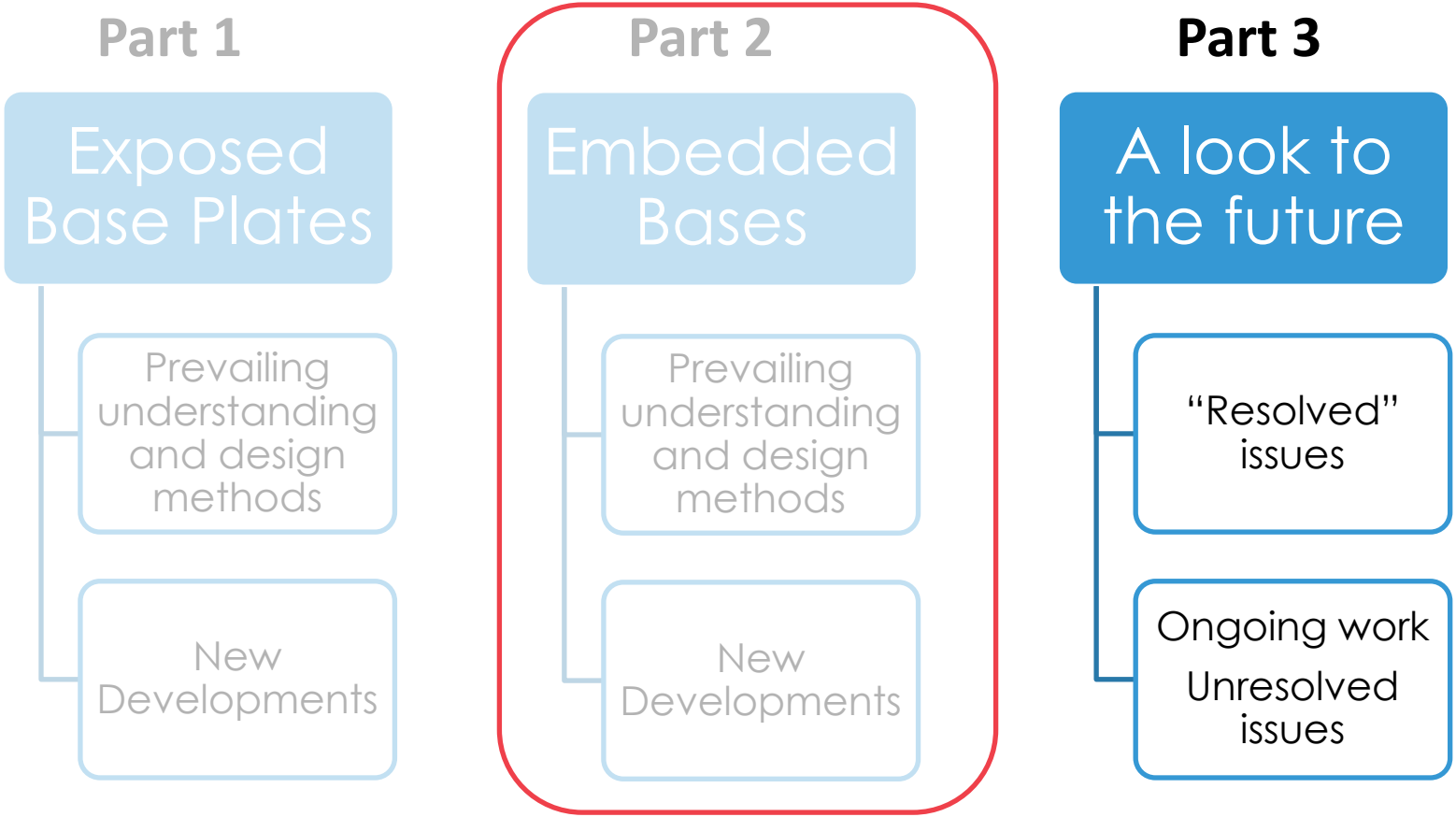


Significant rotation!

Summary – embedded base connections

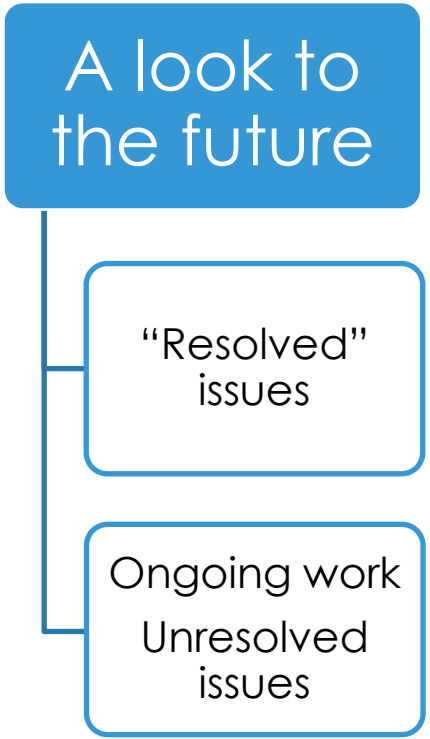
- Knowledge almost entirely new
- Existing methods do not fully capture complexity and mechanisms
- New test data has led to improved methods
- Rotational flexibility is an issue

Organization



A look to the future

Part 3



A look to the future

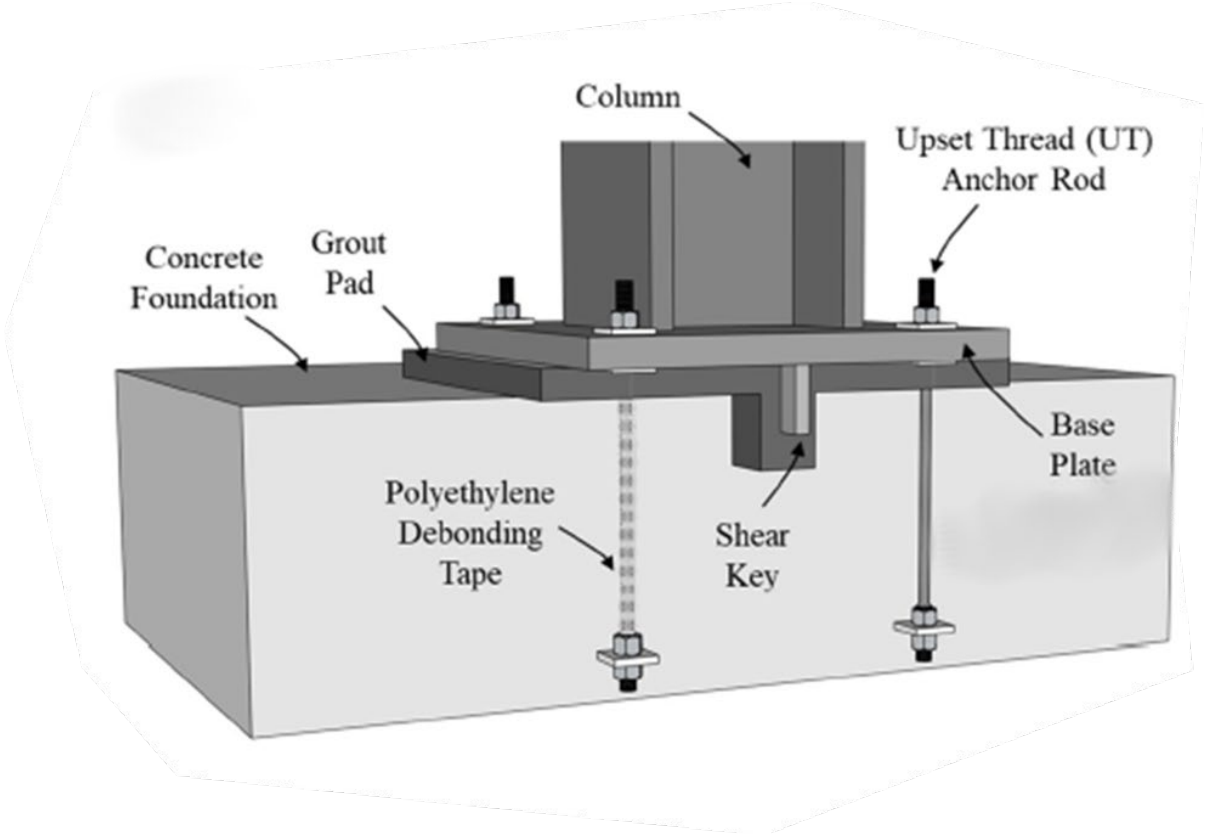
Part 3

A look to the future

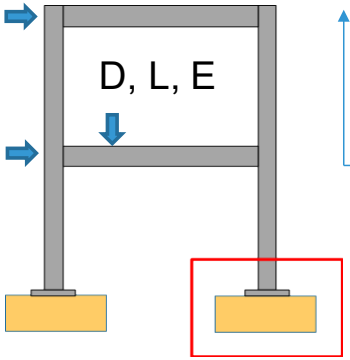
- "Resolved" issues
- Ongoing work
  Unresolved issues

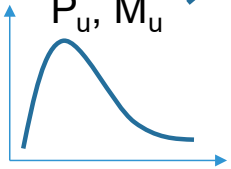
- Minor modifications to strength model
- Ductile details for weak base design
- Reliability analysis
- Biaxial bending
- Anchorages
- Shear transfer
- Alternate anchor rod patterns
- Modeling tools
- Effect of slab overtopping

Ductile details for weak base design

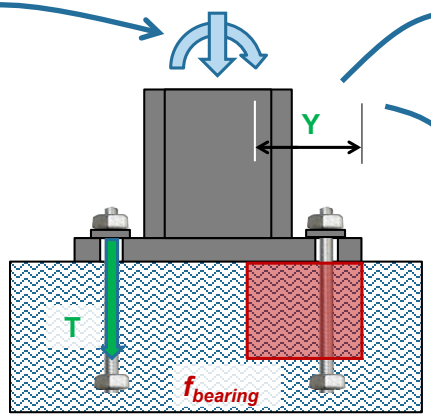


Reliability analysis

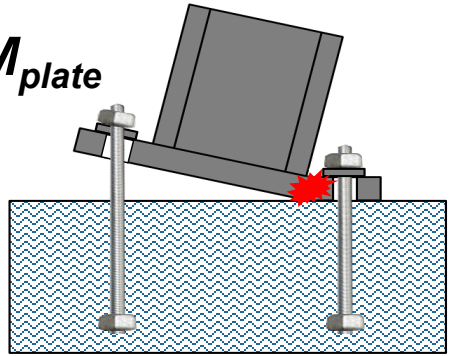




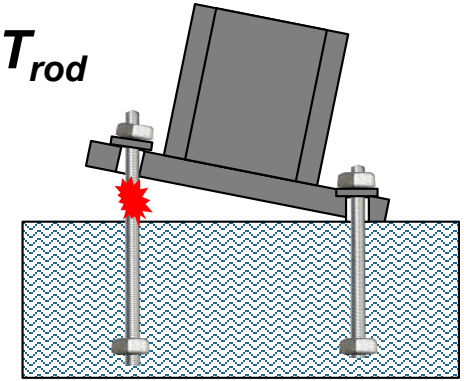
Uncertain component demands



$M < \phi\ M_{plate}$

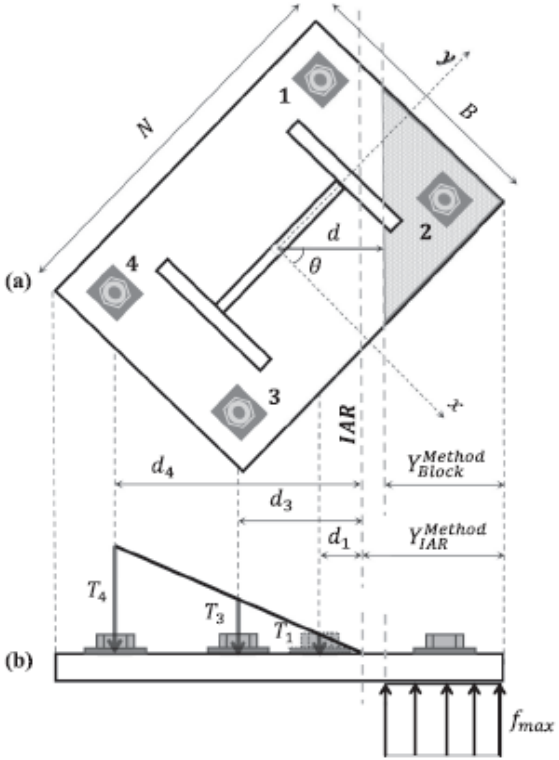


$T < \phi\ T_{rod}$

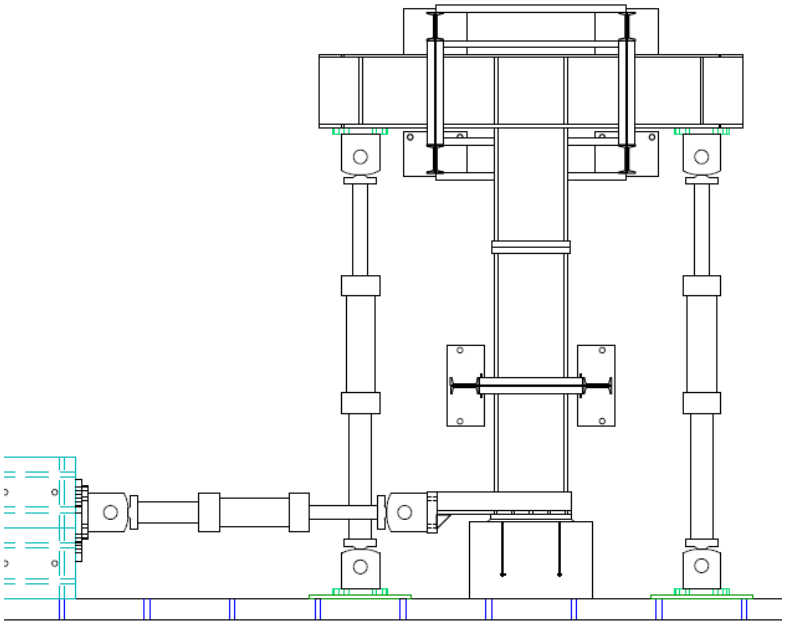


Additional step of calculating sub-component forces

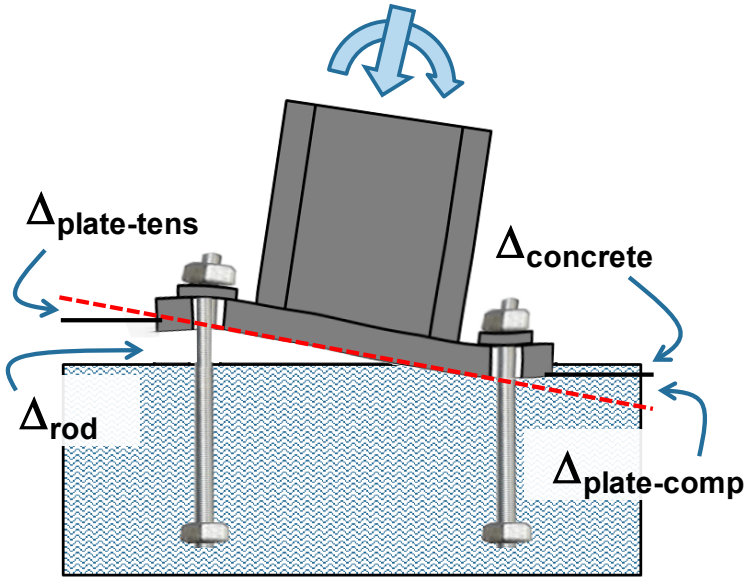
Biaxial bending and alternate rod patterns

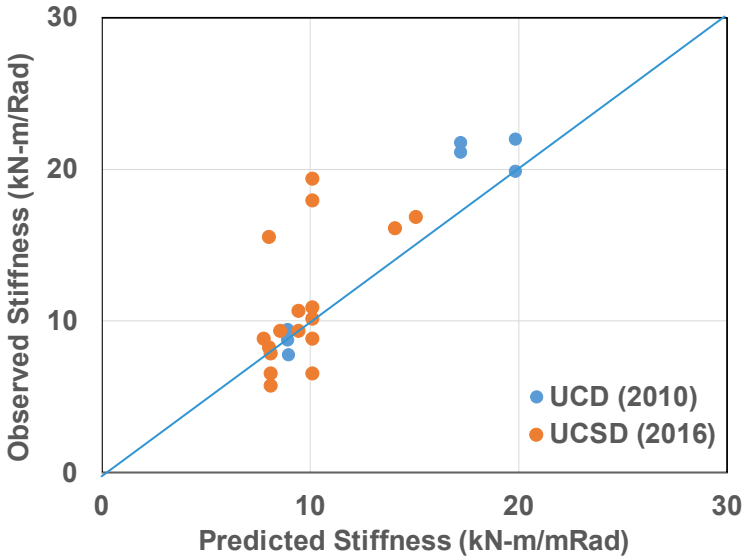


Shear transfer



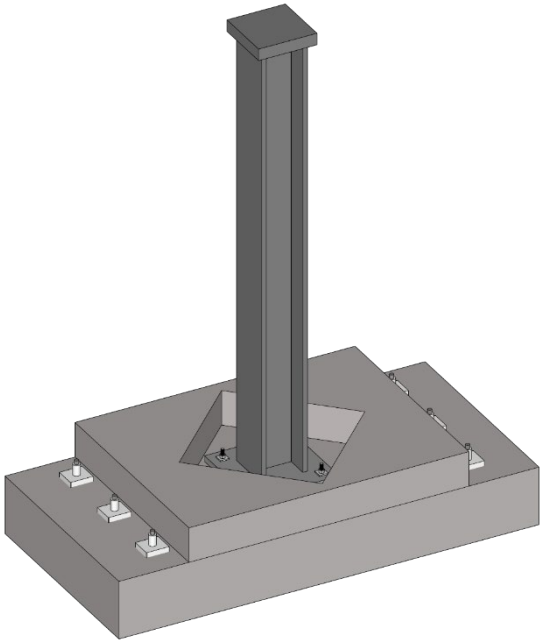
Models for base flexibility – exposed and embedded



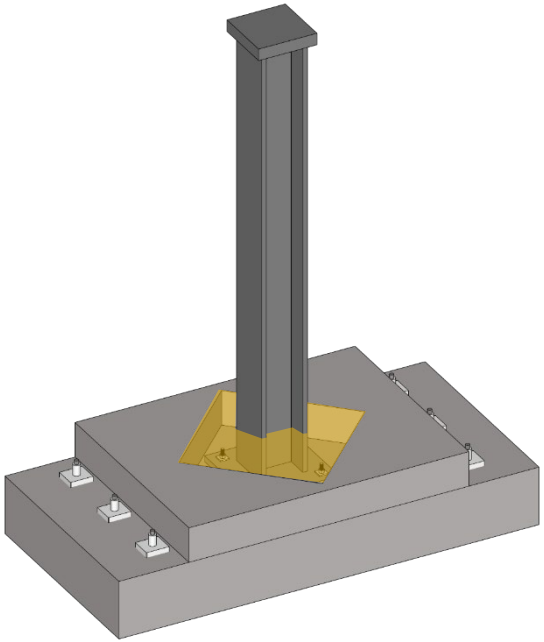


Kanvinde, A.M., Grilli, D.A., and Zareian, F. (2012). "Rotational Stiffness of Exposed Column Base Connections – Experiments and Analytical Models," Journal of Structural Engineering, ASCE, 138(5), 549-560.

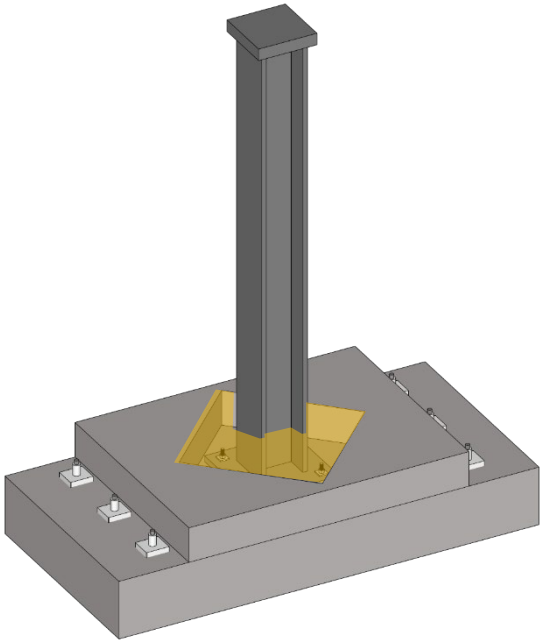
Blockout connections and overtopping slab



Blockout connections and overtopping slab

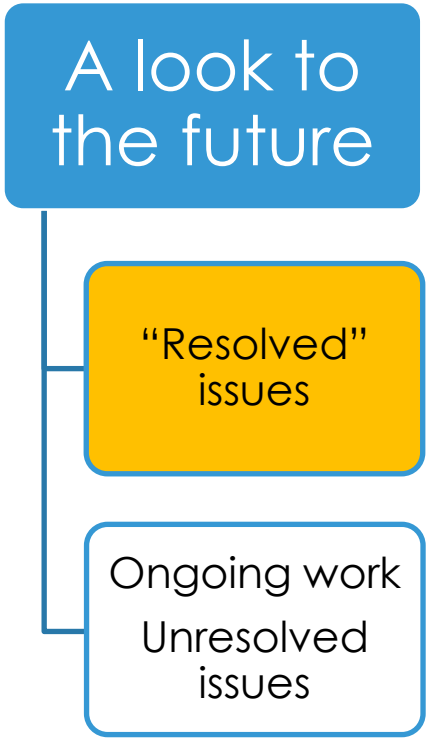


Blockout connections and overtopping slab



Work done at BYU (Paul Richards) and UC Davis

Potential proposals and code changes



- New (3rd) Edition of Design Guide One (~2023) – in progress
- AISC 341 – Next code cycle
- Seismic Design Manual

AISC Design Guide One 3rd Ed

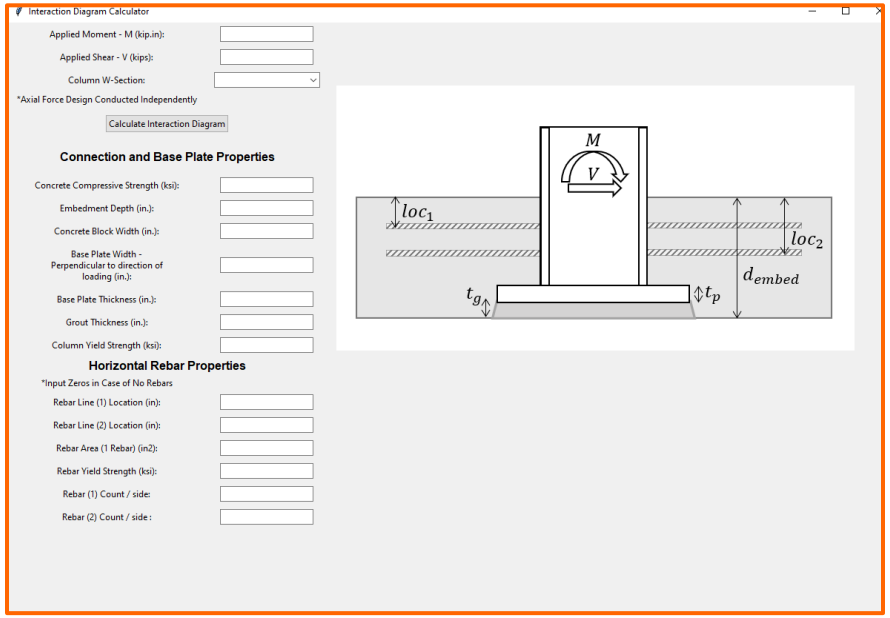
Amit Kanvinde, Mahmoud Maamouri, Josh Buckholt

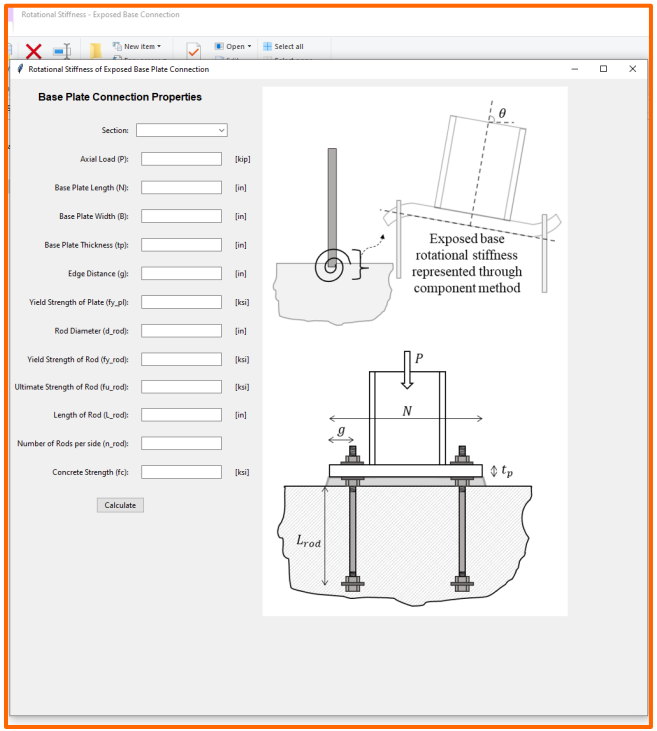
- New chapter on embedded connections
- Detailed consideration of seismic issues
- Configurations not addressed currently (rod patterns, biaxial bending)
- Stiffness models
- Guidelines for computer analysis

AISC Design Guide One 3rd Ed

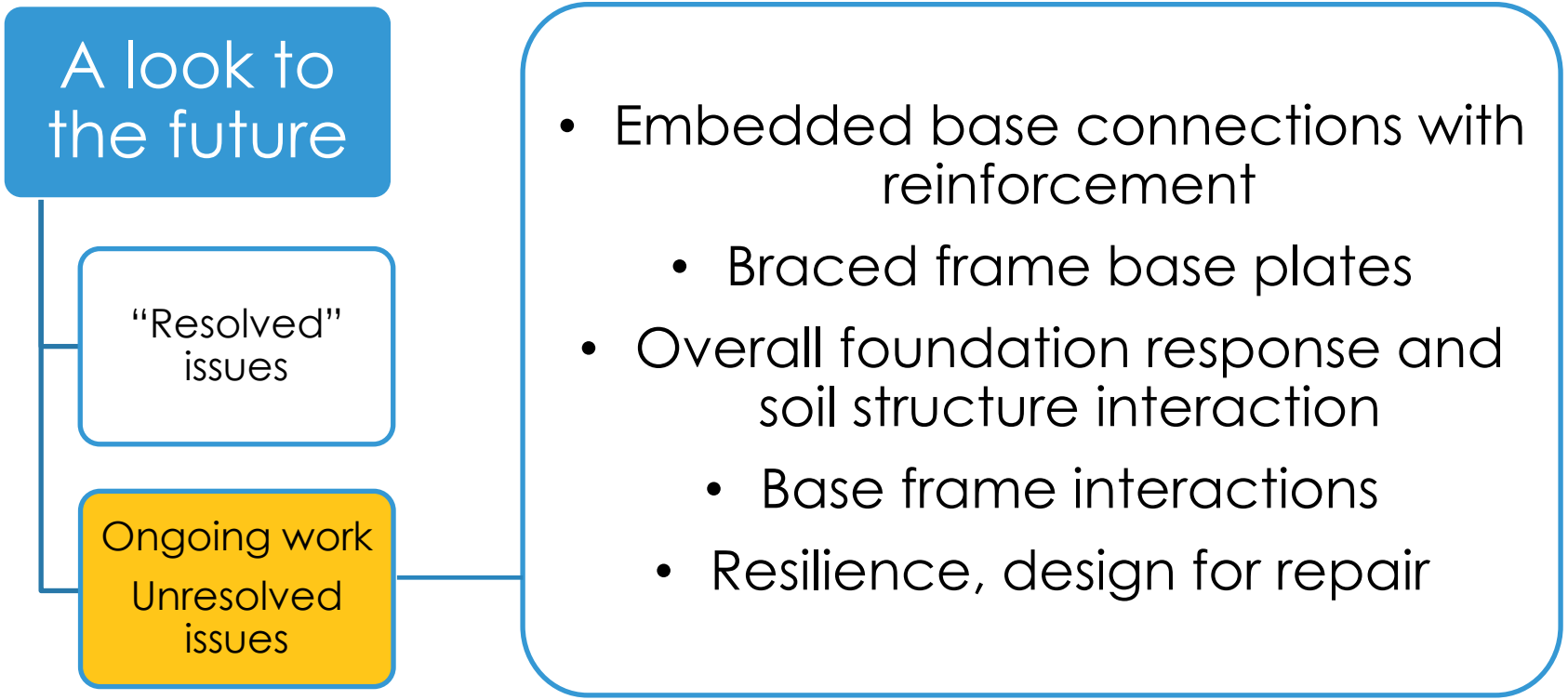
Amit Kanvinde, Mahmoud Maamouri, Josh Buckholt

- Web Tools!





A look to the future



Braced frame base plates

A look to the future

- "Resolved" issues
- Ongoing work
  Unresolved issues

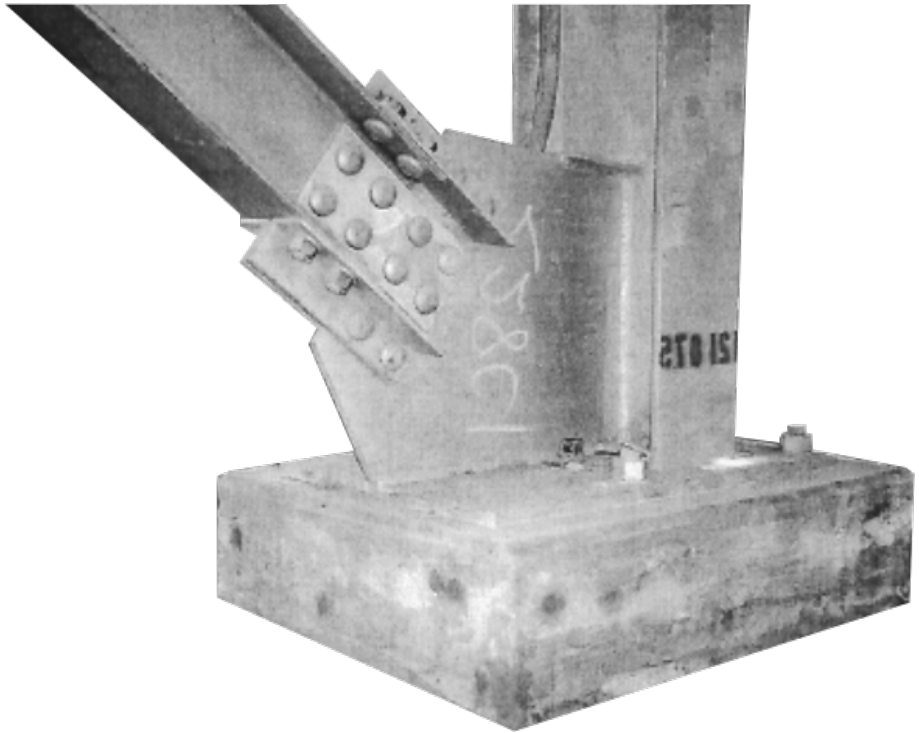
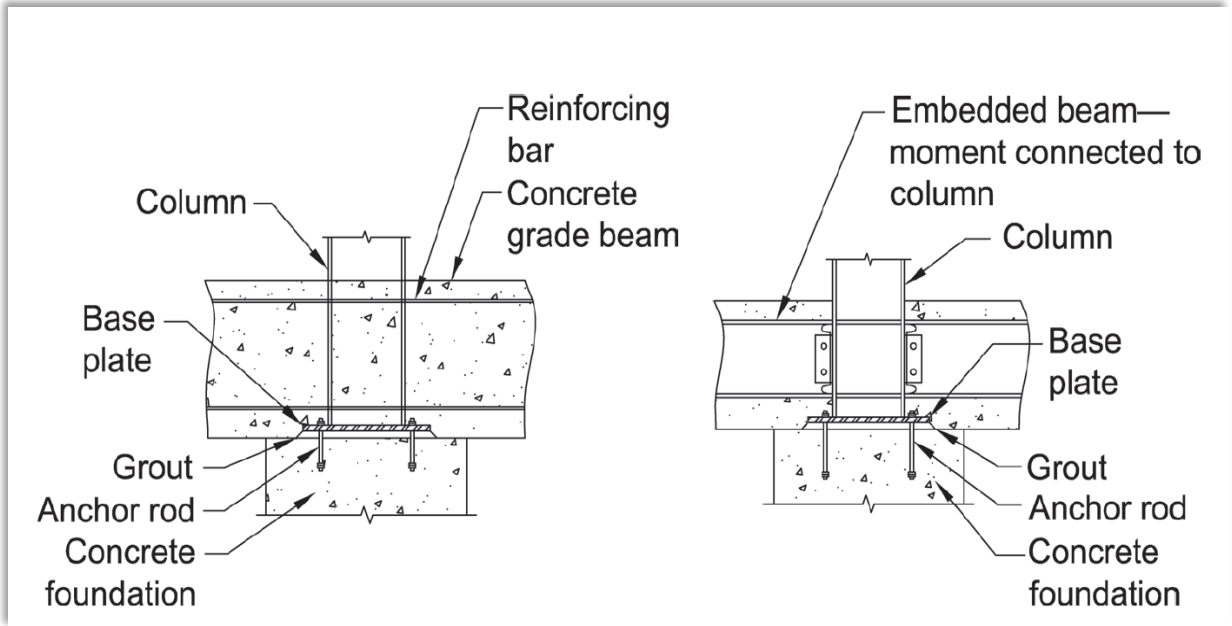


Photo credit: Rick Drake (2003)

Overall foundation response

A look to the future

- "Resolved" issues
- Ongoing work
  Unresolved issues

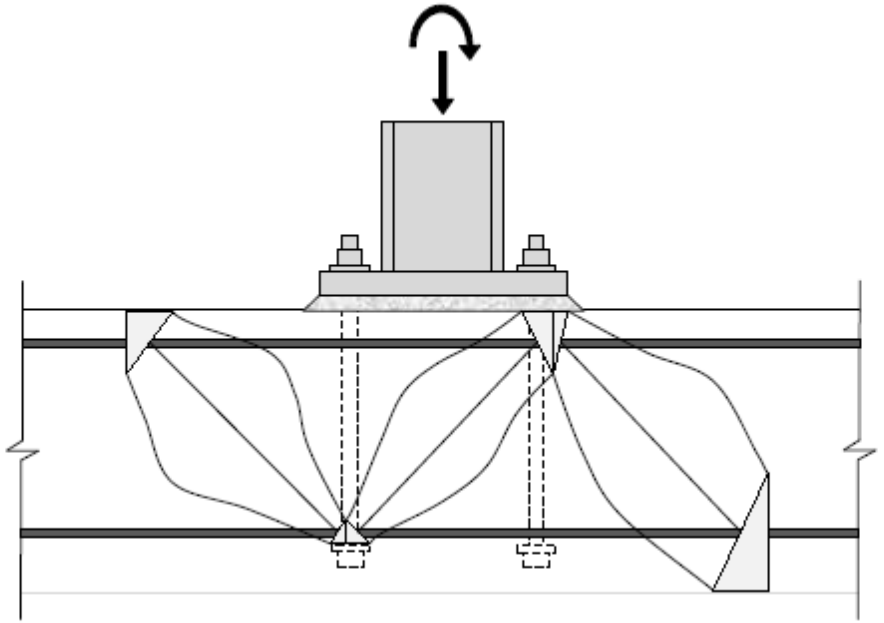


Grade beams

Overall foundation response

A look to the future

- "Resolved" issues
- Ongoing work
  Unresolved issues

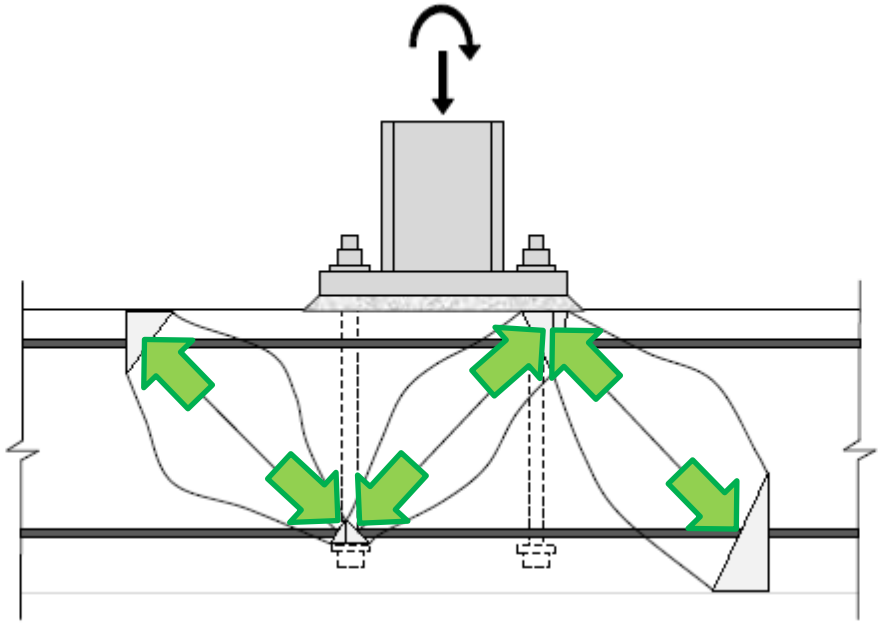


Grade beams and overall foundation response

Overall foundation response

A look to the future

- "Resolved" issues
- Ongoing work
  Unresolved issues

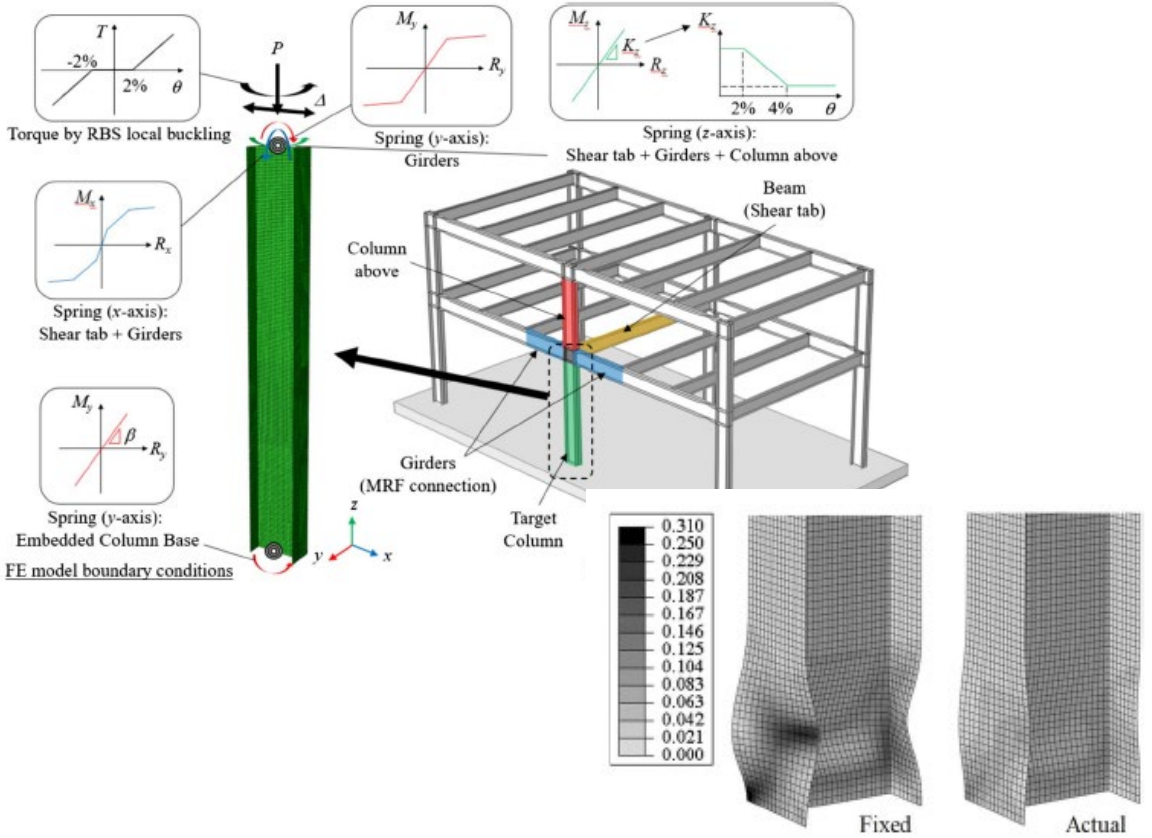


…all the way to soil structure interaction

Base frame interactions

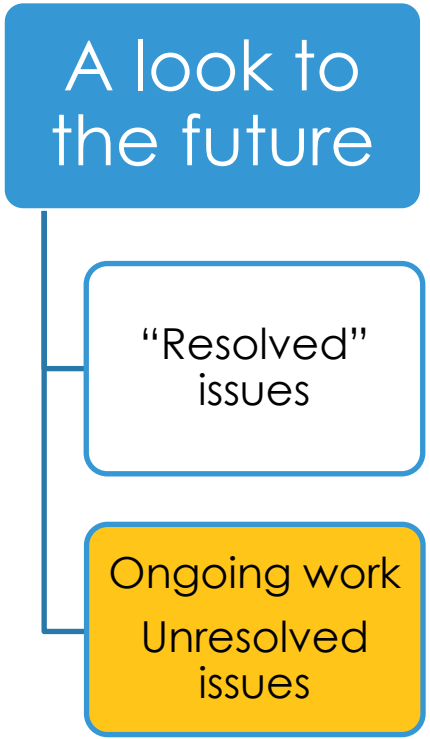
A look to the future

- "Resolved" issues
- Ongoing work
  Unresolved issues



Inamasu, I., Kanvinde, A.M., and Lignos, D., (2019). "Seismic Stability of Wide-Flange Steel Columns Interacting with Embedded Column Base Connections," Journal of Structural Engineering, American Society of Civil Engineers, 145 (12), 04019151.

Still an exciting area with many opportunities



- Resilience and remaining life
- Design to minimize damage
- Design for repair

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Thank you!

https://faculty.engineering.ucdavis.edu/kanvinde/